

D5.3: Simulation and lab-scaled testing of the materials recovery processes

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EXECUTIVE SUMMARY

The main objective of the TREASURE project is to test innovative technologies to make the automotive sector more circular. To this end, TREASURE wants to implement an AI-based scenario assessment tool to support the development of circular supply chains in the automotive industry. Through a series of success stories deriving from applying the principles of the circular economy in three key value chains linked to the automotive sector, TREASURE wants to demonstrate in practice the real benefits deriving from the adoption of circular behavior. Key enabling technologies (KETs) will be integrated into selected processes to support the efficient design of automotive electronics and their subsequent disassembly and material recovery. Deliverable 5.3 "Simulation and lab-scale testing of materials recovery processes" is part of the WP5 "Pilot plants reconfiguration/optimization" activities. The purpose of this document is to provide all the information relating to the laboratory-scale treatment of numerous materials in the automotive sector using hydrometallurgical processes. The document presents a detailed analysis of the characterization of each material in terms of precious and base metal contents. In addition, the results collected, shared and managed through a common Microsoft OneDrive folder have been summarized and incorporated into this document.

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1. Introduction

1.1. Background

The study carried out on the different materials supplied was conducted by analyzing and possibly modifying two patented processes:

- GOLD-REC 1: Process For The Hydrometallurgical Treatment Of Electronic Boards [1].
- GOLD-REC 2: Hydrometallurgical Method For The Recovery Of Base Metals And Precious Metals From A Waste Material [2].

GOLD-REC 1

The current hydrometallurgical procedure consists in the following operations:

- The waste printed circuit boards are firstly subjected to a physical mechanical procedure where the Al- and Fe-based components are removed manually (by using a heat gun) from PCBs surface. Then, the depopulated PCBs are shredded and milled to suitable particles sizes.
- 2. The milled PCBs are then leached with water, sulfuric acid and hydrogen peroxide for the extraction of base metals.
- 3. The separation of the solids from the leach liquid is carried out by filtration process followed by washing with water. The resulted solution (filtrate) is subjected to a precipitation process for Sn precipitation. Then, also this solid precipitate is separated from solution by filtration and further washed with water. The solution achieved after Sn recovery s sent to an electrowinning cell for Cu recovery.
- 4. The resulted solution is recycled in the first leaching for the treatment of another PCB material (counter-current leaching).
- 5. The solid residue of base metals leaching process is involved into another leaching process with thiourea as reagent, ferric sulfate as oxidant in diluted sulfuric acid for Au and Ag dissolution.
- 6. After the separation of the solid from the solution by filtration, the electrowinning process is also applied to this solution for Au and Ag recovery. Once the process is finished, the remaining solution discharged from Au and Ag can be also recycled for the leaching of precious metals for the treatment of other PCBs.

<u>GOLD-REC 2</u>

This hydrometallurgical process could be synthetically described as indicated below:

- 1. The chemical process can be applied on the e-waste without grinding (with whole waste PCBs as an example) avoiding important loss of precious metals also described in the literature.
- 2. The process uses a unique step of metals dissolution with a chemical leaching using HCl, H_2O_2 , acetic acid in water solution at room temperature (21 °C ± 3 °C) with a solid/liquid ratio of 10-20%. The chloroacetic acid is produced by in-situ chemical process within two steps: firstly, hydrochloric acid reacts with hydrogen peroxide and acetic acid to produce peracetic acid, water and chlorine; in the second step chloroacetic acid and hydrochloric acid are produced by the chlorination of the unreacted acetic acid.
- 3. Precious (Au and Ag) and base metals (Cu, Sn, Zn, Ni, Pb) are dissolved leaving the waste PCBs with mainly epoxy resins and fiberglass structure intact (with some residues of metals);

- 4. The liquid solution is easily separated from the S/L system and selective reductionprecipitations steps are considered in the process to recover the dissolved metals. These steps are synthetically described in the follow:
 - Reduction and precipitation of Au chloride to its metallic form by ascorbic acid;
 - Cooling the solution to less than 15 °C for precipitation of AgCl;
 - Selective reduction and precipitation of Cu by metallic Sn or co-reduction of both copper and tin ions with iron metal;
 - Reduction and precipitation of SnCl₂ by metallic Zn;
 - Exploitation of the residual solution for its recycling within the process or by adding iron in order to produce a FeCl₂-FeCl₃ solution useful for coagulation processes in the treatment of wastewaters;
- 5. The main products are: Au (after melting process in an inductive electrical oven adding some slug forming compound), AgCl, Cu and Sn in powder forms (mainly in the range of 10-90 μ m) and a residual chloride solution that can be regenerated by make-up with proper reagents concentration or treated with iron metal to achieve a high concentrated iron solution (extensively and usually utilized in the coagulation processes in wastewater treatments).

1.2. Objectives

The activity was aimed at studying the technical and economic feasibility of using different hydrometallurgical processes on numerous materials. The materials provided by the various partners were analyzed both to assess their intrinsic value and to have an idea of the recovery efficiencies of the hydrometallurgical processes for the extraction of the various precious and base metals contained therein. Below is a table summarizing all the materials analyzed during this activity on a laboratory scale.

Table 1. Summary of all studied materials

| PARTNER SUPPLIER | SOURCE | MATERIAL |
|------------------|------------------|-------------------------------|
| TNO | - | Flexible electronics |
| | | Infotainment, Dashboard, |
| | Seat350 Leon II | Additional Brake Light, |
| | 3eat330 Leon II | Speed and ABS Sensor, Rain |
| | | Sensor, Mirror |
| | | Infotainment, Dashboard, |
| | | Additional Brake Light, |
| SEAT | Seat370 Leon III | Speed and ABS Sensor, Rain |
| 02/11 | | Sensor, Mirror, Rear View |
| | | Mirror |
| | | |
| | | Dashboard, Speed and ABS |
| | Seat250 Ibiza IV | Sensor, Mirror, Rear View |
| | | Mirror |
| | | |
| EuroLCDs | - | Liquid crystal displays |
| | - | Printed circuit boards – AF81 |

2. Characterization

The chemical characterization of the different materials provided by the various partners was performed. The main analysis techniques used are:

• Inductively Coupled Plasma – Optical Emission Spectroscopy (ICP-OES)

This definition identifies an analytical instrument capable of measuring the light (optical emission) produced by a liquid sample when introduced into an inductively coupled argon gas plasma. Through this mechanism it is possible to quantify the metals contained in the sample by measuring, for each one, the intensity of the light emitted with a specific optical bench (system of mirrors, lenses and gratings). For the determination in ICP-OES it is necessary to have samples in liquid form. In this regard, aqua regia leaching is often used to determine the metal content of a solid matrix. Aqua regia is a mixture of nitric acid and hydrochloric acid, optimally in a molar ratio of 1:3.

• <u>X-ray fluorescence spectroscopy (XRF)</u>

XRF is a non-destructive analysis technique which allows to know the elemental composition of a sample through the study of X-ray fluorescence. This radiation is emitted by the atoms of the sample following excitation (which can also give a photoelectric effect), which typically achieved by irradiating the sample with high-energy X-rays and gamma rays. Being a semi-quantitative analysis, it has a lower precision than ICP-OES analyses.

Both techniques allow to know the quantity of metals present in the sample in terms of mass percentage of the element. However, with these procedures it is not possible to know the molecular form in which the metals are present. In order to know the mineralogical form, an X-ray diffraction (XRD) analysis is required.

2.1. Flexible electronics 1 (TNO)

TNO provided samples of Flexible electronics with optically transparent, viscoelastic, chemically and thermally stable composite matrix. In most cases, the substrates (on both sides) are PET. The spacer (in between PET) is either TPU or a commercial material. Figure 1 shows an example of the samples. In this sample, the silver was embedded.



Figure 1. Flex circuit sample

The sample was chemically etched with aqua regia for the determination of the silver content. A mean **Ag concentration of 0.31 wt%** was determined, taking into account the full weight of the sample.

2.2. In-mold electronics 2 (TNO)

In-mold electronics (IME) samples were provided by TNO. The samples mainly consist of plastic sheets with polycarbonate backing and different types of printed layers (black and white graphic inks, dielectrics) and silver paste printed with a polymer binder. D5.6 – "Simulation of the in-mold-structural electronics prototyping process" contains more information describing the device build-up and material composition of each layer. Some samples were not over molded with polycarbonate resin. For these samples, the silver was directly accessible: it is on the surface not embedded by a plastic layer, so can be directly exposed to the action of the acid. Below are presented two examples of the sample (A, B).



Figure 2. In-mold electronics: sample A



Figure 3. In-mold electronics: thermoformed sample B.

The initial concentration of silver in samples A and B was calculated through the analyses carried out on the solutions by ICP-OES.

Table 1. Silver concentration of E-waste – thermoformed samples.

| Ag Concentration (%) | | | |
|-----------------------|------|--|--|
| Thermoformed sample A | 0.36 | | |
| Thermoformed sample B | 0.63 | | |

In addition, also XRF analyses were performed to have qualitative information in order to detect also the other metals. An example of these analyses is provided in Table 2. In the following figures (Figures 4-5) it is possible to see a map showing areas where the analyses were performed; areas were selected by the different colors.



Figure 4. Map of performed XRF analyses for the characterization of sample A.



Figure 5. Map of performed XRF analyses for the characterization of sample B.

Table 3 shows the results obtained from XRF analyses for area 1 of sample A The other results are reported in the Appendix B.

| Ζ | Symbol | Element | Norm. Int. | Concentratio | on | Abs. Erro | л |
|----|--------|--------------|------------|--------------|---------|-----------|-----|
| 12 | Mg | Magnesium | 0.0000 | < 0.0020 | % | (0.0) | % |
| 13 | AI | Aluminum | 73.6823 | < 0.0020 9 | % | (0.0) | % |
| 14 | Si | Silicon | 913.0952 | 0.4782 9 | % | 0.0008 | % |
| 15 | P | Phosphorus | 31,0425 | 0.00623 9 | % | 0.00015 | % |
| 16 | S | Sulfur | 3264.5297 | 0.3101 9 | % | 0.0003 | % |
| 17 | CI | Chlorine | 298.8645 | 0.01104 9 | % | 0.00003 | % |
| 19 | ĸ | Potassium | 44,2475 | 0.01903 9 | % | 0.00021 | % |
| 20 | Ca | Calcium | 49,7790 | 0.00063 9 | % | 0.00001 | % |
| 22 | Ti | Titanium | 125,4881 | 0.01324 9 | % | 0.00009 | % |
| 3 | V | Vanadium | 21.0388 | 0.00141 9 | % | 0.00005 | % |
| 4 | Cr | Chromium | 31,4012 | 0.00111 9 | % | 0.00003 | % |
| 25 | Mn | Manganese | 14116,5111 | 0.4539 9 | % | 0.0003 | % |
| 6 | Fe | Iron | 12076 9126 | 0.6383 | % | 0.0005 | % |
| 7 | Co | Cobalt | 2,4330 | < 0.00017 9 | % | (0.0) | % |
| 8 | NI | Nickel | 45,7436 | 0.00123 9 | % | 0.00002 | % |
| 9 | Cu | Copper | 310,8789 | 0.00672 | % | 0.00003 | % |
| 0 | Zn | Zinc | 22,7999 | 0.00034 9 | % | 0.00001 | % |
| 1 | Ga | Gallium | 0.3439 | < 0.00005 9 | % | (0.0) | % |
| 2 | Ge | Germanium | 0 0000 | < 0.00005 9 | % | (0.0) | % |
| 3 | As | Arsenic | 1 9967 | 0.00002 9 | % | 0.00001 | % |
| 4 | Se | Selenium | 2 5407 | 0.00002 9 | % | 0.00001 | % |
| 5 | Br | Bromine | 4 4707 | < 0.00005 9 | 36 | (0.00003) | % |
| 7 | Bb | Rubidium | 5 8103 | < 0.00005 9 | % | (0.00002) | % |
| 8 | Sr | Strontium | 39 0812 | < 0.00005 9 | % | (0.0) | 9% |
| ğ | Y | Yttrium | 0.0000 | < 0.00005 9 | % % | (0.0) | % |
| 0 | 71 | Zirconium | 0.2934 | < 0.00010 9 | 26 | (0.0) | 9/2 |
| 1 | Nb | Niobium | 0.3178 | 0.00016 9 | % | 0.00007 | % |
| 2 | Mo | Molyhdenum | 0.9827 | 0.00002 9 | 26 | 0.00001 | 9/ |
| 7 | Aa | Silver | 1.0365 | 0.00007 9 | 26 | 0.00003 | % |
| 8 | Cd | Cadmium | 2 0584 | 0.00008 9 | 26 | 0.00001 | 96 |
| 0 | Sn | Tin | 3 4910 | 0.00428 9 | 20 | 0.00050 | 04 |
| 1 | Sh | Antimony | 1 1930 | < 0.000420 | /0 % | (0.0) | 04 |
| 2 | Te | Tellurium | 3 0040 | < 0.00030 9 | N/ | (0.0) | 9/ |
| 3 | 1 | lodine | 0.0000 | < 0.00030 | 10 | (0.0) | 94 |
| 5 | Ce | Cocium | 0.0000 | < 0.00040 9 | NG. | (0.0) | 0/ |
| 6 | Ba | Barium | 2 3420 | < 0.00040 9 | 26 | (0.0) | 96 |
| 7 | La | Lanthanum | 2 2980 | < 0.00020 9 | 26 | (0.0) | 96 |
| 8 | Ce | Cerium | 2 1024 | < 0.00020 9 | % | (0.0) | 94 |
| 9 | Dr | Praseodymium | 8 9735 | 0.00146 9 | 24 | 0.00012 | 9/ |
| 0 | Nd | Neodymium | 17 4217 | 0.00241 9 | 26 | 0.00012 | 0/ |
| 2 | Hf | Hafnium | 4 2243 | < 0.00010 9 | 20 | (0.0) | 96 |
| 2 | Ta | Tantalum | 27 5725 | < 0.00010 | 26 | (0.0) | 0/ |
| 4 | W | Tungsten | 20377 | < 0.00010 | 26 | (0.0001) | 9% |
| - | Ha | Mercupy | 3.0540 | 0.00002 | 24 | 0.00001) | 94 |
| 14 | TI | Thallium | 4.5074 | 0.00004 | n0 | 0.00001 | 0/ |
| 1 | Dh | Inallum | 4.53/4 | 0.00004 | 70 | 0.00001 | 70 |
| 2 | PD | Lead | 6.8112 | 0.00011 9 | 70 | 0.00001 | 70 |
| 3 | BI | Bismuth | 0.0000 | < 0.00010 | 70 | (0.0) | 70 |
| NU | In | Inonum | 7.1449 | 0.00007 9 | 70 | 0.00001 | 70 |
| 52 | U | Uranium | 5.0199 | < 0.00010 | % | (0.0) | % |

Table 2. XRF of thermoformed sample A, area 2

2.3. Car components (SEAT)

SEAT has supplied automotive components for 3 different types of cars: SEAT 350 LEON II, SEAT 370 LEON III and SEAT IBIZA IV. The choice of the models and of the car components comes from a thermodynamic rarity assessment (D3.1). Table 3 summarizes the various components received with the relative codes and quantities.

| SEAT 350 LEON II | Qty. | SEAT 370 LEON III | Qty. | SEAT IBIZA IV | Qty. |
|---------------------------|------|------------------------|------|-------------------------|------|
| INFOTAINMENT | х3 | INFOTAINMENT | x3 | - | - |
| DASHBOARD | x2 | DASHBOARD | x2 | DASHBOARD | x3 |
| ADDITIONAL BRAKE LIGHT | x3 | ADDITIONAL BRAKE LIGHT | x2 | - | - |
| SPEED AND ABS SENSOR | x3 | SPEED AND ABS SENSOR | x3 | SPEED AND ABS SENSOR | x3 |
| RAIN SENSOR | x3 | RAIN SENSOR | x2 | - | - |
| - | - | MIRROR | x3 | MIRROR | x3 |
| - | - | REAR VIEW MIRROR | x3 | REAR VIEW MIRROR | x3 |

Table 3. Car components received from SEAT

Each of the above components has been disassembled into its sub-components using the instructions provided by SEAT. Disassembly times were similar to those expected by SEAT. Subsequently, each sub-component was weighed by means of a technical balance and photographed.

Table 4. Example of the disassembly of the seat Leon II dashboard

| Ν. | Photo | Weight [g] | wt % | Materials |
|----|-------|------------|--------|-----------|
| 0 | | 844.2 | 100% | - |
| 1 | | 239.1 | 28.32% | Plastic |

| 2 | 198.9 | 23.56% | See Table 6 |
|---|-------|--------|------------------|
| 3 | 197.9 | 23.44% | Plastic Glass |
| 4 | 192.7 | 22.83% | Plastic |
| 5 | 11.2 | 1.33% | Plastic |

| 6 | | 3.0 | 0.36% | Plastic |
|-------|---|-------|--------|----------|
| 7 | | 1.2 | 0.14% | Aluminum |
| Total | - | 844.0 | 99.98% | - |

A detailed analysis of the metal content was carried out for the electronic boards (component n. 2 of Table 5) of the dashboard of each SEAT model. In this respect, the connection devices, the transducers, the electromagnets, the display devices and the display board have been removed from the electronic board. Subsequently, the grinding with a knife mill of the board was carried out. Leaching with aqua regia or nitric acid was performed for each removed component and ground fraction. ICP-OES analyzed the resulting solution to determine the content of the different precious and base metals of interest. The following tables show the results obtained for each car model.

| | | | g/ton | | | wt | % |
|----------------------|-------|-------|-------|-------|-------|-------|------|
| Components | wt % | Au | Ag | Pd | Ті | Cu | Sn |
| Powders | 66.52 | 59.08 | 169.0 | 19.20 | 715.7 | 11.54 | 1.05 |
| Transducer | 4.41 | 12.38 | 2.40 | - | - | 3.96 | 0.56 |
| Electromagnets | 23.01 | 11.48 | 0.01 | - | - | 0.10 | 1.73 |
| Connection device | 3.68 | 3.73 | 130.7 | 8.60 | 4.84 | 18.13 | 1.42 |
| Display device | 0.30 | 748.5 | 868.0 | 42.30 | 11.94 | 21.54 | 3.11 |
| Display board | 0.27 | 684.5 | 648.5 | - | - | - | 2.39 |
| Losses | 1.81 | | | | | | |
| Tot. | 100.0 | | | | | | |

Table 5. Characterization dashboard electronic board SEAT Leon II

| | | | g/t | on | | wt | % |
|----------------------|-------|-------|-------|-------|-------|-------|------|
| Components | wt % | Au | Ag | Pd | Ti | Cu | Sn |
| Powders | 72.89 | 27.77 | 244.3 | 9.48 | 683.7 | 14.47 | 0.98 |
| Transducer | 6.20 | 1.59 | 1.05 | - | - | 6.43 | 2.30 |
| Inductor | 3.33 | - | 81.10 | - | 50.35 | 20.62 | 0.64 |
| Electromagnets | 12.07 | 0.08 | 0.00 | - | - | 43.84 | 0.10 |
| Connection device | 4.26 | - | 86.60 | 3.47 | 72.96 | 1.06 | 0.31 |
| Display device | 0.34 | 0.12 | 1389 | 0.00 | - | 21.54 | 3.11 |
| Display board | 0.00 | 0.91 | 513.1 | 75.12 | - | 22.01 | 2.10 |
| Losses | 0.91 | | | | | | |
| Tot. | 100.0 | | | | | | |

Table 6. Characterization dashboard electronic board SEAT Leon III

Table 7. Characterization dashboard electronic board SEAT Ibiza IV

| | | | g/ | ton | | wt | % |
|--------------------|-------|-------|-------|------|------|-------|------|
| Components | wt % | Au | Ag | Pd | Ti | Cu | Sn |
| Powders | 73.33 | 61.87 | 265.3 | 29.1 | 1637 | 20.46 | 1.23 |
| Transducer | 5.94 | 14.36 | 66.2 | - | - | 4.90 | 2.10 |
| Electromagnet s | 14.75 | 0.00 | 2.50 | - | - | 0.52 | 0.09 |
| Connection device | 5.02 | 3.02 | 84.41 | 6.59 | 0.78 | 18.32 | 1.52 |
| Losses | 0.96 | | | | | | |
| Tot. | 100.0 | | | | | | |

The non-metallic fractions of the electronics boards are composed to fiber glass, epoxy resin and plastics [5].

2.4. Liquid crystal displays – ITO glass (EuroLCDs)

The samples were provided by EUROLCDs in the scope of TREASURE project (task 5.3 – lab scale activities). Figure 6 shows the photographic aspect of the sample.



Figure 6. LCD – ITO GLASS 2x3 cm pieces

The sample was attacked by aqua regia, and the resulting solution was subsequently analyzed by ICP-OES to determine the content of the metals of interest: In and Sn. The study of these two metals was dictated by literature analyses and by economic/critical interest [3].

Table 8 summarizes the composition of ITO glasses in terms of metals. Indium and tin were present as oxides.

| Chemical attack | Mass [g] | In [g/t] | Sn [g/t] |
|----------------------------------|----------|----------|----------|
| 1. double step aqua regia attack | 4.032 | 71.12 | 25.17 |
| 2. single step aqua regia attack | 3.834 | 60.90 | 8.87 |

Table 8. Chemical composition of ITO glasses (ICP-OES analysis).

The chemical composition was also defined by performing XRF analysis. The main components are shown in the following table. In addition to indium and tin were found only elements due to the glass.

Table 9. Chemical composition of ITO glass (XRF analysis)

| Elements | Concentration |
|----------|---------------|
| Si | 37.9 % |
| Mg | 4.4 % |
| Са | 4.8 % |
| S | 1.6 % |
| In | 60 -70 g/t |
| Sn | 15 - 20 g/t |

The other detected elements (K and P) have a concentration below 1 %.

2.5. Liquid crystal displays – printed circuit boards (EuroLCDs)

EuroLCDs has supplied Printed Circuit Boards (PCBs). Figure 7 shows an example of the sample.



Front side

Back side



Figure 7. PCBs Sample (AF81)

All the components on the board were detached, by heating and manual removal, in order to chemically characterize each type. Table 10 and Table 11 shows the results of this analysis. Then, the components have been processed using different methods to solubilize metals. The quantitative analyses were performed by inductively coupled plasma optical emission spectrometry (ICP-OES) on the solutions obtained by the chemical attacks. In this way it was possible to characterize the metallic fraction of the sample.

| List of components | | | | |
|--------------------------------|----------------------|-------|-------|--|
| co | components weight, % | | | |
| inductors | inductors C102 | 22.58 | 27.06 | |
| Inductors | inductors DR73 | 5.38 | 27.96 | |
| hack papals | back panels | 10.33 | 12.26 | |
| back panels | back panels' hooks | 1.93 | 12.26 | |
| integrated circuit chips (ICC) | | 2 | .08 | |

Table 10. Summary of component and relative percentage by weight

| resisters | resistors | 0.50 | 0.83 | |
|-----------------------------------|---|----------------|---------------|--|
| resistors | chip resistors | 0.32 | 0.82 | |
| t | ransistors | 8.55 | | |
| capacitors | multilayer ceramic capacitors (MLCC) | 3.39 | | |
| | tantalum capacitors | 0.49 | 4.10 | |
| | solid state capacitors | 0.22 | | |
| | sensors | 0.36 | | |
| electronic oscillator - amplifier | | 0.11 | | |
| board without components | | 43.20 | | |
| | | total: 99.44 % | | |
| | | loss of mat | erial: 0.56 % | |

Table 11. Results of components metal fraction characterization (ICP-OES analysis), expressed as element mass concentration

| | INDUCTORS (C 102) weight: 22.58 % | | | | |
|--|--|-------------------------------|--|--|--|
| | Cu: 33.6 % Fe: 1.27 % Zn: 0.17 % | Cr: 471.6 g/t Ag: 62.1 g/t | | | |
| | Cu: 89.1 % | Cr: 1252 g/t | | | |
| | Fe: 3.37 % | Ag: 164.9 g/t | | | |
| THE A | Zn: 0.45 % | | | | |
| description: black ceramic box with a copper wire internally | | | | | |
| All the second | other materials (62.3 %): plastics, ceramic materials, ferrite | | | | |
| | qualitative analysis: Sn | | | | |

method: they were broken and then the inner coil was submitted to aqua regia digestion

| | INDUCTORS (DR73) weight: 5.38 % | |
|--|--|---------------|
| | Cu: 18.7 % | |
| | Fe: 1.44 % | |
| | Ni: 1.40 % | Ag: 142 4 g/t |
| | Sn: 1.00 % | Ag. 145.4 g/t |
| | Pb: 0.76 % | |
| | Zn: 0.39 % | |
| | description: plastic/ceramic box with an inner copper coil and Sn-Ag solders other materials: plastics, ceramic qualitative analysis: Ca, Si | |

| method: they were broken and then the inner coil was submitted to aqua regia digestion | | | | | |
|--|-------------------------------------|---------------------|--|---|--|
| E | LECTRONIC OSCILLATOR – A | MPLIFIER (TXC bo | rde) | | |
| | weight: 0.1 | 11% | | | |
| | Fe: 13.7 % | | | | |
| ttt | Ni: 9.71 % | | Δσ | · 3675 3 g/t | |
| | Sn: 1.47 % | | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | · 191 2 α/t | |
| | Cu: 0.32 % | | AL | 1. 101.2 g/t | |
| | | | | | |
| TH | othe | er materials: ceram | ic, quart | Z | |
| | | qualitative analysi | s: Co | | |
| | method: aqua reg | ia digestion | | | |
| | BACK PAN | ELS | | | |
| | weight: 10. | 05 % | | | |
| <u>Ria</u> | St. As | Cu: 87.9 % | | Ag: 1260.7 g/t | |
| All III | PAR | Sn: 0.91 % | | Au: 1136.2 g/t | |
| | and a state | Ni: 0 48 % | | Pd: 132.4 g/t | |
| NE BRA | 8- | 7n: 0.48 % | | Pb: 49.8 g/t | |
| | ¥ | | | Al: 13.3 g/t | |
| \sim | | qua | litative a | analysis: Zr | |
| method: they w | vere manually broken and th | en submitted to ac | qua regia | adigestion | |
| | | Cu: 48.4 % | | | |
| | | Zn: 38.9 % | | Pd: 3068.6 g/t | |
| 10 | | B: 24.5 % | | Au: 963.8 g/t | |
| | 1 million | Al: 3.19 % | | Δg· 213 5 g/t | |
| | | Sn: 3.02 % | | A_{g} . 213.3 g/t Dh· 17.2 g/t | |
| 1 | 12 | Ni: 0.44 % | | 1 D. 47.2 g/t | |
| | | Ti: 0.14 % | | | |
| blue bac | k panel | qualitative a | inalysis: | Ca, K, Na, Sb, Si, Zr | |
| | | Cu: 24.7 % | | Zn: 561.4 g/t | |
| | | B: 2.92 % | | Au: 196.8 g/t | |
| | | Sn: 1.14 % | | Ag: 89.8 g/t | |
| | | Al: 1.07 % | | Pb: 16.2 g/t | |
| - | | Ni: 0.62 % | | Pd: 14.1 g/t | |
| | | | | | |
| black bac | ck panel | qualitative an | alysis: C | a, Na, K, SD, SI, TI, Zr | |
| | | Cu: 48.4 % | / D | | |
| | | 7n: 19.5 % | <u>,</u> | | |
| | | B' 18 6 % | - - | Au: 243.6 g/t | |
| h. | 1 | ΔΙ· 3 13 % | | Ag: 196.4 g/t | |
| | | Sn: 1 2/1 % | | Pb: 28.2 g/t | |
| 1.00 | | Ni: 0 10 % | | | |
| box back panel | | | , ve analv | sis: Na K Pd Si | |
| | qualitative analysis: Na, K, Pd, Si | | | 515. Hu, K, Fu, 51 | |
| method: aqua regia digestion | | | | | |
| | WHITE BACK PANELS | | | | |
| | | | | Ni: 423 0 g/t | |
| | Cu: 2.97 % | | | Δσ· 260 7 σ/τ | |
| | Sn: 0.30 % | ,) | | , ι ₆ . 200.7 g/τ Διι· 39 9 σ/τ | |
| | | | | πα. 33.3 g/ ι | |

| | other materials: plastics qualitative analysis: Pd | | |
|------------|---|--|--|
| | method: aqua regia digestion | | |
| | BACK PANELS' HOOKS | | |
| | weight: 1.93 % | | |
| | Cu: 39.9 % Zn: 26.5 % | Ag: 620.2 g/t Ni: 416.0 g/t | |
| | method: agua regia digestion | 15. 511 | |
| | | | |
| | | | |
| THE LEFT | Cu: 15.8 % Zn: 3.27 % Sn: 0.92 % Ni: 0.26 % | Ag: 1714 g/t Pd: 1516 g/t Au: 76.4 g/t | |
| | description: plastic/ceramic box with a gold screw inside and Sn-Ag solders other materials: plastics, ceramic qualitative analysis: Al, Pb | | |
| method: th | hey were broken and then submitted to aqua r | egia digestion | |
| | INTEGRATED CIRCUITS -CHIPS (ICC) | | |
| | weight: 2.08 % | | |
| | Cu: 40.2 % Sn: 1.99 % Zn: 0.31 % Ni: 0.23 % | Au: 3688.5 g/t Ag: 319.6 g/t Pd: 103.1 g/t | |
| - A A | other materials: pl | astics | |
| | qualitative analysis: Al, B | a, Ca, Fe, Pb | |
| method: | they were cut and then submitted to aqua reg | ia digestion | |
| | RESISTORS | | |
| | weight: 0.50 % | | |
| | Cu: 26.6 % | | |
| | Sn: 3.30 % | | |
| 2000 | B: 2.36 % | Ag: 689.4 g/t | |
| ST ALLO | Ni: 0 11 % | | |
| | qualitative analysis: Al, | Ba, Ca, Sb | |

| | TRANSISTORS - (VBT) | | |
|--|---|--------------------------------------|--|
| | weight: 8.55 % | | |
| | Cu: 52.0 % | Ag: 414.7 g/t | |
| | Sn: 1.06 % | Au: 78.9 g/t | |
| The Party of the P | AI: 0.32 % | Pd: 46.6 g/t | |
| | Zn: 0.27 % | Ni: 27.6 g/t | |
| VET304E AVE SECTOR | | | |
| | | | |
| VET3045C | other materials: silicon, | ceramic (28 %) | |
| 100 11 | qualitative analys | sis: Pb, Si | |
| | | | |
| method 1: they were brol | ken and then submitted to aqua regia digest | ion (detection of Cu, Sn, Al, Ni) | |
| method 2: they were submit | ted to thermal treatment with Na ₂ CO ₃ (same | e amount as components) at 1060 | |
| °C for 1 h, then the melted | components were quickly cooled, and then | metallic alloy was submitted to | |
| | aqua regia digestion (detection of Au, Ag, | Pa) | |
| | CHIP RESISTORS - (R001 - W) | | |
| | weight: 0.32 % | | |
| * * | Cu: 47.5 % | Al: 584.0 g/t | |
| a lite of | Mn: 5.62 % | Pd: 490.8 g/t | |
| | Ni: 5.05 % | Ag: 483.6 g/t | |
| | Sn: 4.19 % | Pb: 300.2 g/t | |
| | | Ta: 65.6 g/t | |
| 5 | other materials: | plastics | |
| | qualitative anal | ysis: In | |
| Ø 1992 - | description: plastic and solders on the s | surface with inner electrode in | |
| | precious me | etal | |
| method: th | ney were broken and then submitted to aqua | a regia digestion | |
| | SOLID STATE CAPACITORS | | |
| | weight: 0.22 % | | |
| | Cu: 31.4 % | | |
| | Sn: 2.75 % | Ag: 605.6 g/t | |
| | Ti: 1.60 % | Au: 302.1 g/t | |
| | Fe: 0.25 % | Pd: 71.8 g/t | |
| | | | |
| | other mater | rials: ceramic | |
| | qualitative analys | is: Al, Ba, Ca, Er, Ni | |
| | description: ceramic co | omponents with solders | |
| | method: aqua regia digestion | | |
| | TANTALUM CAPACITORS | | |
| | weight: 0.49 % | | |
| | | Ag: 1647 g/t | |
| | | Ta: 126.3 g/t | |
| | Cu: 35.9 % | Pd: 72.2 g/t | |
| | | Au: 28.4 g/t | |
| | | Mn: 19.3 g/t | |
| | other materials: | ceramic | |
| | qualitative analysis: Al | , K, Pb, Sn, Zn | |
| | description: ceramic components with solo | ders on two sides, inside there is a | |
| | tantalum electrode | | |

method: they were broken, then were submitted to 1 hour thermal treatment at 350°C with KOH (two times the amount of solid), then the sample was dissolved in water at 90 °C for 1 h for the detection of Ta and Mn, the solid residue was submitted to nitric acid digestion for Ag and Cu detection and then to aqua regia digestion for Pd and Ru detection.

| | MULTI LAYER CERAMIC CAPACITORS (MLCC weight: 3.39 % |) |
|--|--|--|
| | Ti: 10.23 % Cu: 3.29 % Nb: 0.49 % | Ag: 309.7 g/t Au: 15.5 g/t Pd: 6.3 g/t |
| | other materials: ceramic qualitative analysis: Al, Ba, Ca, Fe, K, Dy, Mg, Ni, Si, Sn, Sr, Ti, Y, Zn, Zr | |
| method: they were broken, t times the amount of solid), the | hen were submitted to 1 hour thermal treat in the sample was dissolved in water at 90 °C | ment at 350 °C with KOH (two C for 1 h for the detection of Nb, |

the solid residue was submitted to nitric acid for Ag and Cu digestion and then to aqua regia digestion for Au. Pd and Ti detection

| BOARD WITHOUT COMPONENTS weight: 43.20 % | | | |
|---|-----------|--|--|
| front side | back side | | |
| | | | |

| | nowders above to 2 mm bave an average size of | |
|--|---|--|
| powders below to 2 mm | the particles of 5 mm, and 8-9 mm as maximum | |
| | size | |
| Overall chemical composition of both fracti | ons (below to 2 mm and above to 2 mm) | |
| Cu: 35.1 % Ag: 616.7 g/t | | |
| Sn: 2.61 % | Pd: 68.9 g/t | |
| B: 1.35 % | Au: 46.6 g/t | |
| other materials: fiber glass, plastics | | |
| qualitative analysis: Al, Ca, Fe, Ni, Zn | | |
| method: the board was cut and then grinded by a cut mill with a 2 mm grid; they were obtained two | | |
| fractions, one below to 2 mm (75.7 %) and the other one above to 2 mm (24.3 %). The obtained powders | | |
| were submitted to sampling and further digestion by aqua regia, three replications were performed. | | |

The following figures are respectively the composition of PCBs in terms of components present (Figure 8) and in terms of metal content (Figure 9).



Figure 8. Weight distribution of PCBs components (normalized to 100 %)



Figure 9. PCBs metals composition (normalized to 1)

3. Process recycling (lab-scale tests)

3.1 Flexible electronics 1 (TNO)

The flexible sensors (Figure 1) were subjected to two successive leaching steps (GOLD-REC1):

- 1. <u>Dimethylformamide (DMF) Leaching</u> aims to dissolve the plastic and facilitate access to the metal parts
- 2. The subsequent extraction of silver by Thiourea Leaching (Thiourea 20 g/L, Fe₂(SO₄)₃ 22 g/L, H₂SO₄ 0.2 mol/L)

Iron from oxidation state +3 is reduced to oxidation state +2 leading to the oxidation of the silver which forms the complex (Ag (SC(NH₂)₂)₃)⁺ with thiourea (SC(NH₂)₂). SC(NH₂)₂ also partially reacts with Fe³⁺ leading to the formation of formamide disulfide (C₂H₆N₄S₂) which decomposes into SC(NH₂)₂, cyanamide (CN₂H₂) to sulfur.

Leaching of silver occurs according to the following chemical reactions:

| $Ag + Fe^{3+} + SC(NH_2)_2 \rightarrow (Ag(SC(NH_2)_2)_3)^+ + Fe^{2+}$ | (1) |
|--|-----|
| 2 SC(NH ₂) ₂ + 2 Fe ³⁺ → C ₂ H ₆ N ₄ S ₂ + 2 Fe ²⁺ + 2 H ⁺ | (2) |
| $2 C_2 H_6 N_4 S_2 \rightarrow SC(NH_2)_2 + CN_2 H_2 + S$ | (3) |

The residual silver content in solid material after thiourea leaching, was measured by attacking it with by use of aqua regia. Figure 10 shows the scheme of the process and Table 12 shows the results obtained.



Figure 10. Simplified process scheme for flexible electronics 1

| DMF | treatment | Thiourea treatment | Acid Attack |
|---|---|--------------------------------------|---|
| Ag content in initial solid sample, % | Ag content in solid sample after DMF treatment, % | thiourea leaching Ag, mg/L | Ag content after Thiourea leaching, % |
| 0.31 | 9.9 | 31.5 | 0.025 |

Table 12. Metal average content after Thiourea Leaching and Acid Attack

The thiourea leaching led to an Ag recovery yield of about 96.7%.

Evaporation treatment has been studied to evaluate the effectiveness of a possible thermal treatment process for spent DMF. For testing, a laboratory rotary evaporator was used.

DMF was inserted into an evaporation flask that was immersed in a thermostatic bath to keep the solution at the appropriate temperature (Heidolph Rotavapor G3). The application of a depression helps to lower the boiling temperature of the solvents. Under vacuum, the solvents boil, and then evaporate, at lower temperatures than they would need working at atmospheric pressure. Furthermore, the rotation of the flask, creating a veil of solution, continuously renewed on the surface of the flask, allows to further increase the evaporation speed. The solvent vapors are removed and condense on contact with the cold surface of a coil in which cold mains water is made to flow. The condensate is collected in droplets in the collecting flask.

The test was carried out at a temperature of 68 $^{\circ}$ C working under vacuum (0.140 bar), the duration of the test was 30 min.

Table 13 shows the Fourier-transform infrared spectroscopy (FTIR²) spectra of the solid part of spent DMF after evaporation. Absorption spectrum of liquid part of spent DMF samples (distillate) (initial, after leaching and distillate after evaporation) were measured using UV–visible spectrophotometer (Table 14).

| Sample | Spent DMF after leaching | After evaporation (recycled DMF) | |
|--------|---|---|--|
| DMF | -0.1468 Helkod Name 5 Jan ARS BaseLine DR Filter BaseLine DR Filter BaseLine DISFLAT PATE | 1996 237.83 NT | |
| | 0.0000 | | |
| | 0.4000 | | |
| | 200.00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 400/00 | 600.00 \$800.00 mt : 200.00 → 800.00 + Label Roce | |

Table 13. UV-VIS spectrum of Spent DMF after leaching and after evaporation

 $^{^2}$ FTIR is a technique used to obtain an infrared spectrum of absorption or emission of a solid, liquid, or gas.



Comparison of the absorption spectra of the sample of DMF before leaching (baseline) with the spectra of samples of spent DMF (Table 14) shows that in all cases of spent DMF, after the leaching process, absorption maxima are observed at 280 and 348 nm. A similar pattern was observed for all spent DMF solutions after the leaching of studied spent flex circuits samples, although the ratio of intensities is somewhat different. It demonstrates the presence of dissolved impurities in the spent solution.

Instead, recycling the spent DMF solution by evaporation makes it possible to almost completely separate the dissolved impurities from the DMF distillate and thus allow its reuse in the leaching process.

The FTIR method carried out an analysis of the concentrate resulting from evaporation. Based on the FTIR spectra (Table 15), depending on the kind of flex circuits samples, after the leaching process, different chemicals were dissolved by DMF: Poly(acrylonitrile: MMA), 7,2-CHLOROETHYLTHEOPHYLLINE IN KB, Poly(ether-ester urethane) MBI, Polyurethane resin, Poly(ether-ester urethane) MBI, POLYETHERURETHANE, Poly(ester urethane).



Table 14. FTIR spectra of the solid part of spent DMF after evaporation

3.2 In-mold electronics 2 (TNO)

A series of experimental tests were carried out to develop a process for the recovery of silver from the polycarbonate-based IME samples (A, B). The samples were submitted to lab-scale activities without reducing the size. The plastic frame was removed.

3.2.1 Thiourea leaching

For sample A, tests with three stages of thiourea leaching were performed: for each stage fresh leaching solutions were used.

Operative conditions:

- thiourea 20 g/L
- ferric sulphate 22.46 g/L
- H₂SO₄ 0.2 mol/L
- pulp density 10 % w/v
- no stirring
- time 1 h.

Leaching of silver occurs according to reactions (1-3).





Table 15. Results of silver dissolution by three stages of thiourea leaching for sample A

| solid residue (98.9 % with respect to the initial solid) | Ag 156 ± 10 g/t |
|--|--------------------|
| reconstituted feed | Ag 0.3623 ± 0.001% |

For sample B, tests with two stages of thiourea leaching were performed: for each stage fresh leaching solutions were used.

Operative conditions:

- thiourea 20 g/L
- ferric sulphate 22.46 g/L
- H₂SO₄ 0.2 mol/L
- pulp density 10 % w/v
- no stirring
- time 1 h

Table 16. Results for sample B

| LEACHING OPERATIONS | | | | |
|--|-------|------|--|--|
| TREATMENT Ag [mg/L] Ag dissolution (%) | | | | |
| thiourea first step – 1 h | 502.0 | 65.0 | | |
| thiourea second step – 1 h | 197.8 | 90.7 | | |

Table 17. Results of silver dissolution by three stages of thiourea leaching for sample B

| solid residue (99.2 % with respect to the initial solid) | Ag 587 g/t | |
|--|-------------|--|
| reconstituted feed | Ag 0.6284 % | |

In the next figure, a simplified scheme of the leaching process for the treatment of sample A was shown.



Figure 12. Simplified process scheme for leaching operation (sample A)

3.2.2 Thiourea leaching without oxidant agent

For sample B, tests with three stages of thiourea leaching were performed without using the <u>oxidant agent</u>: for each stage fresh leaching solutions were used.

Operative conditions:

- thiourea 20 g/L
- H₂SO₄ 0.2 mol/L
- pulp density 10 % w/v
- no stirring
- time 1 h

Table 18. Results of silver dissolution by three stages of leaching without oxidant agent* for sample B

| LEACHING OPERATIONS | | | | |
|---|------|-----|--|--|
| TREATMENT Ag [mg/L] Ag cumulative dissolution (%) | | | | |
| thiourea* first step – 1 h | 19.5 | 2.4 | | |
| thiourea* second step – 1 h | 14.6 | 4.2 | | |
| thiourea* third step – 1 h | 9.9 | 5.4 | | |

The results showed that no significant Ag dissolution occurred performing thiourea leaching without the oxidant agent (Fe^{3+}).

3.2.3 Electrowinning – recovery of silver from the solution

Tests will be performed with electrodes of different materials and shapes. The figure below shows the photographic aspect of one of the tests performed.



Figure 13. Photographic aspect of electrolysis test 4

The reactions that occur during electrolysis are as follows:

| Ag $(SC(NH_2)_2)^{3+}$ + 3 e ⁻ \rightarrow Ag + 3 $(SC(NH_2)_2)$ | (1) |
|---|-----|
| $3 C_2 H_6 N_4 S_2 + 3 H^+ + 3 e^- \rightarrow 3 SC(NH_2)_2$ | (2) |

The really important aspect that is noticed is the regeneration of the TU. In fact, thanks to this process it is possible to greatly reduce the amount of TU necessary for the process with consequent reduction of OPEX.

| TEST | solution | electrodes | operative conditions | results | purity of the obtained powder |
|------|--|---|--|--|-------------------------------------|
| n. 1 | thiourea first step sample A (320 mg/L, volume 80 mL) | cathode and anode: copper, cylindrical shape | voltage: 1.5 V current density: 13 A/m ² | recovery: 65 % time: 2 h energetic consumption: 1.5 kWh/kg | Ag 68.1 % (as metal) |
| n. 2 | thiourea first step sample A (328 mg/L, volume 80 mL) | cathode and anode: copper, cylindrical shape | voltage: 2.0 V current density: 37 A/m ² | recovery: 61 % time: 2 h energetic consumption: 4.8 kWh/kg | n.a. |
| n. 3 | thiourea first step sample A (317 mg/L, volume 80 mL) | cathode: copper anode: graphite cylindrical shape | voltage: 1.5 V current density: 62 A/m ² | recovery: 79 % time: 2 h energetic consumption: 5.0 kWh/kg | n.a. |
| n. 4 | thiourea first step sample B (500 mg/L, volume 90 mL) | cathode: copper anode: graphite cylindrical shape | voltage: 1.2 V current density: 43 A/m ² | recovery: 95 % time: 2 h energetic consumption: 2.9 kWh/kg | Ag 75.4 % (as metal) |

Table 19. Summary of electrowinning tests

The experimental tests, summarized in Table 19, allowed to identify the best operative conditions for the recovery of silver from the leaching solution by electrodeposition.

Cylindrical electrodes must be immersed in the solution to ensure good mixing of the solution in the equipment. Copper was used as cathode because in this case the silver powder can be directly obtained in the metallic form without a subsequent thermal refining phase [7]; graphite, instead, was used as anode. A silver recovery of 95 % occurred at the following conditions: voltage 1.2, current density 43 A/m². In Figure 14 is shown the silver recovery and current efficiency calculated at different times of test 4.



Figure 14. Silver recovery and current efficiency at different times of test 4

In the obtained powder was determined a grade of silver of around 75 %, graphite was detected as main impurity, probably due to the degradation of the anode.

In Figure 15 the X-Ray diffraction analysis of the obtained silver powder was showed. From the analysis the intensity of the peaks of silver as a metal is greater than that of silver as an oxide.



Figure 15. X-Ray diffraction analysis performed on silver powder (test 4)

3.2.4 Cross-leaching process

In order to study the cross-leaching process an iodometric titration method to detect the content of thiourea, Fe³⁺ and formamidine disulfide (FDS) was used. In addition, also a titration acid-base was performed to evaluate the sulfuric acid concentration. The results showed the opportunity to reuse the solution after the first step of leaching for the treatment of the same solid (second step of leaching) with a chemical make-up. After the electrodeposition operation, the solution was again titrated. So, the solution, discharged by the silver, can be reused for a new batch in the same way. The solutions can be recycled in 3 batches before disposing of as wastewater.

3.3 Car components (SEAT)

Several leaching tests were performed to evaluate the recovery efficiency of Au, Ag, Pd, Cu and Sn through Gold-Rec1 and Gold-Rec2 processes on the dashboard components of the various SEAT cars. The Printed Circuit Boards (PCBs) powders obtained by grinding with a knife mill as described in chapter 4.2 were subjected to the Gold-Rec1 process. The other components were treated with the Gold-Rec2 process.

Based on the Au content, the technical feasibility of the grinding and the background of UNIVAQ [4-6] it was decided to treat the components with high Au concentrations (i.e. Au > 300 ppm) with Gold-Rec2 without any reduction dimensional while the residual parts were ground and treated with powders using Gold-Rec1.

In addition, some components must be removed as they inhibit the recovery of gold, others cannot be subjected to grinding and others with high Cu concentrations lead to a significant increase in operating costs. Some of these components are batteries, Al electrolytic capacitors, Quartz oscillators or Inductors. Components with high copper concentrations are not convenient to treat with a hydrometallurgical process and a pyrometallurgical treatment is preferred.

3.3.1 PCBs powders Leaching

The conditions of the tests carried out on the powders are the following:

- Solid concentration 15% wt./vol.
- Mixing 200 rpm
- H₂O₂ 20% vol.
- H₂SO₄ 10% vol.
- Thiourea 20 g/L
- Ferric sulphate 22.46 g/L

The tests carried out were structured on 3 steps each. The first two 90 min steps for the leaching of the base metals and the third 60 min step for the leaching of gold and silver by thiourea. Table 20 shows the results obtained in terms of recovery yields.

| Model | Extraction yields | Step I | Step II | Step III | Total |
|----------|-------------------|--------|---------|----------|-------|
| | Au | 0.5% | 0.0% | 48.7% | 48.7% |
| Loop II | Ag | 4.5% | 0.8% | 43.8% | 43.8% |
| Leon II | Pd | 71.6% | 0.0% | 8.5% | 8.5% |
| | Cu | 87.1% | 7.5% | 0.3% | 94.6% |
| | Au | 1.8% | 0.0% | 58.8% | 58.8% |
| | Ag | 14.5% | 0.3% | 54.0% | 54.0% |
| Leon III | Pd | 63.7% | 10.8% | 8.5% | 8.5% |
| | Cu | 80.7% | 9.8% | 0.2% | 90.5% |
| | Sn | 8.8% | 3.5% | 0.5% | 12.2% |
| | Au | 0.0% | 0.0% | 61.7% | 61.7% |
| | Ag | 37.5% | 28.2% | 21.1% | 21.1% |
| Ibiza IV | Pd | 53.6% | 13.6% | 8.9% | 8.9% |
| | Cu | 83.5% | 14.0% | 0.1% | 97.5% |
| | Sn | 86.7% | 3.3% | 0.4% | 90.0% |

Table 20. Extraction yields for different car model powders

The obtained leaching yields are relatively low if compared with the yields obtained with the same process on materials very similar to those used. Some differences on yield of extraction from the models depend on the different components on the boards.

In this regard, the studied process is to be studied in more detail for its optimization. Unfortunately, the time available from the time of arrival of the materials did not allow for this in-depth analysis. The process optimization will be completed in the D5.4.

3.4 Liquid crystal displays (EuroLCDs)

A series of experimental tests was carried out starting from a literature review [3] in order to develop a process for the recovery of indium and tin. Preliminary tests aimed at evaluating the necessity of a preliminary treatment to free metals from coating's layers. Hence, before a test with acetone treatment before leaching operation was compared with that carried out without preliminary treatment.

3.4.1 Preliminary tests

TEST I. Acetone preliminary treatment - sulfuric acid leaching

This preliminary test was performed to understand the behavior of this material in different situations. Washing using acetone and water is necessary for the removal of the protective layer covering the metals in order to make them accessible during the leaching phase with sulfuric acid.

| | STAGE | OPERATIVE CONDITIONS |
|---|--------------------|-----------------------------------|
| | washing by acetone | solid concentration 10 % wt./vol. |
| 1 | solid 10.124 g | time 90 min, |
| | volume 101 mL | stirring 250 rpm |
| 2 | washing with water | washing on the filter |
| 2 | volume 100 mL | washing of the filter |

Table 21. Operative conditions for TEST I

| | sulfuric acid leaching | sulfuric acid 2 mol/L |
|---|---|--|
| 3 | solid 10.110 g | solid concentration 10 % wt./vol. |
| | volume 100 mL | stirring 250 rpm, temperature 60 °C, time 60 – 90 min. |
| 4 | washing water in 2 steps/(15 mL and 15 mL) | washing on the filter |
| - | chemical attack of solid | time 120 min |
| Э | residue by aqua regia | temperature 90 °C |

Table 22. Results for TEST I

| STAGE | | | YIELD OF DISS | OLUTION (%) |
|-------|-------------------------------------|--|---------------------------------|---------------------------------|
| | STAGE | RESULIS | In | Sn |
| 1 | washing by acetone | Loss of weight: 0.14% | - | - |
| 2 | washing by water | - | - | - |
| 3 | sulfuric acid leaching | 1h: In 6.84 mg/L – Sn 0.88 mg/L 1h30: In 3.28 mg/L – Sn 1.12 mg/L | 1h: 98.5% 1h30: 52.4% | 1h: 52.5% 1h30: 74.5% |
| 4 | washing water 1 washing water 2 | 1: In 1.47mg/L – Sn 0.93 mg/L 2: In 0.41 mg/L – Sn 0.23 mg/L | - | - |
| 5 | chemical attack of solid residue | _ | - | - |

Reconstituted feed: In: 68.60 g/t - Sn: 16.55 g/t.

TEST II. Direct sulfuric acid leaching

Table 23. Operative Conditions for TEST II

| | STAGE | OPERATIVE CONDITIONS |
|---|--|--|
| 1 | sulfuric acid leaching solid 9.961 g volume 100 mL | sulfuric acid 2 mol/L solid concentration 10 % w/v, stirring 250 rpm, temperature 60 °C, time 1h – 1h30. |
| 2 | Washing with water 30 mL | washing on the filter |
| 3 | chemical attack of solid residue by aqua regia | time 2 h temperature 90 °C |

Table 24. Results for TEST II

| STAGE | | DECILITC | YIELD OF DISSOLUTION (%) | | | |
|-------|-------------------------------------|--|--------------------------------|--------------------------------|--|--|
| | | REJULIS | In | Sn | | |
| 1 | sulfuric acid leaching | 30': In 3.36 mg/L – Sn 1.16 mg/L 1h In 5.10 mg/L – Sn 1.88 mg/L | 30': 54.9% 1h: 80.6% | 30': 37.8% 1h: 65.0% | | |
| 2 | washing water | In 0.92 mg/L – Sn 0.75 mg/L | - | - | | |
| 3 | chemical attack of solid residue | - | - | - | | |

Reconstituted feed: In: 61.50 g/t - Sn: 30.80 g/t.

3.4.2 Leaching tests: factorial design plan

Three factors are selected to carry out the factorial design plan with central composite: temperature, sulfuric acid concentration and pulp density. Every leach operation is carried out for 1.5 h. In the following table are shown their coded names and their high, mid and low levels.

| Factor | Coded Name | Low level (-) | Mid level (0) | High Level (+) |
|--------------------------------|------------|---------------|---------------|----------------|
| Temperature | A | 25 °C | 42,5°C | 60 °C |
| H ₂ SO ₄ | В | 1 mol/L | 1,5 mol/L | 3 mol/L |
| Solid % | С | 5 % wt/vol | 10 % wt/vol | 15 % wt/vol |

Table 25. Coded names and levels

The following tables shows the results.

Table 26. Dissolution yields for indium obtained from factorial design plan

| test | Α | В | с | AB | AC | BC | ABC | A^2 | B^2 | C^2 | In dissolution, % |
|------|--------|--------|--------|----|----|----|-----|---------|---------|---------|-------------------|
| 1 | -1 | -1 | -1 | 1 | 1 | 1 | -1 | 1 | 1 | 1 | 0,91 |
| 2 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 | 1 | 98,91 |
| 3 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | 1 | 1 | 0,58 |
| 4 | 1 | 1 | -1 | 1 | -1 | -1 | -1 | 1 | 1 | 1 | 99,85 |
| 5 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | 1 | 1 | 2,37 |
| 6 | 1 | -1 | 1 | -1 | 1 | -1 | -1 | 1 | 1 | 1 | 99,29 |
| 7 | -1 | 1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | 1 | 5,05 |
| 8 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 99,69 |
| 9 | -1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 0 | 1,25 |
| 10 | 1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 0 | 99,92 |
| 11 | 0 | -1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 4,37 |
| 12 | 0 | 1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 23,18 |
| 13 | 0 | 0 | -1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 4,1 |
| 14 | 0 | 0 | 1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 10,28 |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9,25 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9,31 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7,53 |

Table 27. Significative factors for indium dissolution

| | Coefficients | Standard error | Stat t | Significance value | Less then 95% | More then 95% | 1-p | Significance |
|-----------|--------------|----------------|--------|--------------------|---------------|---------------|------|--------------|
| Intercept | 7,02 | 13,90 | 0,51 | 0,63 | -26,98 | 41,03 | 0,37 | 36,87 |
| Α | 40,62 | 6,53 | 6,22 | 0,00 | 24,65 | 56,59 | 1,00 | 99,92 |
| В | 2,59 | 6,53 | 0,40 | 0,71 | -13,38 | 18,56 | 0,29 | 29,44 |
| С | 1,21 | 6,53 | 0,19 | 0,86 | -14,76 | 17,18 | 0,14 | 14,11 |
| AB | -0,13 | 8,53 | -0,01 | 0,99 | -20,99 | 20,74 | 0,01 | 1,13 |
| AC | -0,71 | 8,53 | -0,08 | 0,94 | -21,58 | 20,15 | 0,06 | 6,40 |
| BC | 0,31 | 8,53 | 0,04 | 0,97 | -20,56 | 21,17 | 0,03 | 2,77 |
| ABC | -0,44 | 8,53 | -0,05 | 0,96 | -21,31 | 20,42 | 0,04 | 3,98 |
| A^2 | 20,59 | 7,18 | 2,87 | 0,03 | 3,01 | 38,16 | 0,97 | 97,14 |
| B^2 | 7,58 | 7,18 | 1,06 | 0,33 | -10,00 | 25,15 | 0,67 | 66,80 |
| C^2 | 5.25 | 7.18 | 0.73 | 0.49 | -12.32 | 22.83 | 0.51 | 50.77 |

As it's shown in the previous table, the temperature results to be the only significative factor with a positive effect on the dissolution yield of indium. Also, a response curve can be developed from those results.



Figure 16. Response curve for indium dissolution yield

Table 28. Dissolution yields for tin obtained from factorial design plan

| test | Α | в | с | AB | AC | BC | ABC | A^2 | B^2 | C^2 | Sn dissolution, % |
|------|--------|--------|--------|----|----|----|-----|---------|---------|---------|-------------------|
| 1 | -1 | -1 | -1 | 1 | 1 | 1 | -1 | 1 | 1 | 1 | 76,62 |
| 2 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 | 1 | 22,16 |
| 3 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | 1 | 1 | 73,22 |
| 4 | 1 | 1 | -1 | 1 | -1 | -1 | -1 | 1 | 1 | 1 | 68,02 |
| 5 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | 1 | 1 | 9,2 |
| 6 | 1 | -1 | 1 | -1 | 1 | -1 | -1 | 1 | 1 | 1 | 47,02 |
| 7 | -1 | 1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | 1 | 14,36 |
| 8 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 90,71 |
| 9 | -1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 0 | 82,46 |
| 10 | 1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 0 | 87,59 |
| 11 | 0 | -1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 14,12 |
| 12 | 0 | 1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 0 | 67,15 |
| 13 | 0 | 0 | -1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 72,22 |
| 14 | 0 | 0 | 1,682 | 0 | 0 | 0 | 0 | 0 | 0 | 2,82912 | 19,28 |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11,49 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20,48 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12,09 |

Table 29. Significative factors for tin dissolution

| | Coefficients | Standard error | Stat t | Significance value | Less then 95% | More then 95% | 1-p | Significance | 1-p | Significance |
|-----------|--------------|----------------|--------|--------------------|---------------|---------------|--------|--------------|------|--------------|
| Intercept | 15,30 | 5,82 | 2,63 | 0,04 | 1,07 | 29,53 | 1,07 | 29,53 | 0,96 | 96,10 |
| A | 4,62 | 2,73 | 1,69 | 0,14 | -2,06 | 11,30 | -2,06 | 11,30 | 0,86 | 85,86 |
| В | 13,22 | 2,73 | 4,84 | 0,00 | 6,53 | 19,90 | 6,53 | 19,90 | 1,00 | 99,71 |
| с | -12,28 | 2,73 | -4,50 | 0,00 | -18,97 | -5,60 | -18,97 | -5,60 | 1,00 | 99,59 |
| AB | 10,97 | 3,57 | 3,08 | 0,02 | 2,24 | 19,70 | 2,24 | 19,70 | 0,98 | 97,82 |
| AC | 21,73 | 3,57 | 6,09 | 0,00 | 13,00 | 30,46 | 13,00 | 30,46 | 1,00 | 99,91 |
| BC | 0,80 | 3,57 | 0,22 | 0,83 | -7,93 | 9,53 | -7,93 | 9,53 | 0,17 | 16,97 |
| ABC | -1,34 | 3,57 | -0,38 | 0,72 | -10,07 | 7,39 | -10,07 | 7,39 | 0,28 | 28,01 |
| A^2 | 22,75 | 3,01 | 7,57 | 0,00 | 15,39 | 30,10 | 15,39 | 30,10 | 1,00 | 99,97 |
| B^2 | 7,06 | 3,01 | 2,35 | 0,06 | -0,30 | 14,41 | -0,30 | 14,41 | 0,94 | 94,28 |
| C^2 | 8,86 | 3,01 | 2,95 | 0,03 | 1,51 | 16,22 | 1,51 | 16,22 | 0,97 | 97,44 |

As it's shown in the previous table, the sulfuric acid concentration and pulp density result to be significative factors respectively with a positive and a negative effect on the dissolution yield of indium; interactions between temperature and sulfuric acid concentration and between temperature and pulp density also result to be significative with a positive effect. Also, a response curve can be developed from those results.



Figure 17. Response curve for tin dissolution yield

In order to maximize indium dissolution yield, because it's the precious metal, the best run results to be AC (T=60 °C; H2SO4 concentration= 1 mol/L; pulp density= 15 % wt/v) with a dissolution yield of 99.29 % for indium and 47.02 % for tin. Also, this run was chosen as the best one because it allows to reduce sulfuric acid consumption and to increase process potential.

To further reduce reagents consumption other tests with a sulfuric acid concentration of 0.5 mol/L were carried out. The dissolution yields were found to be very similar to the best run ones, so the perfect choice is to work with a sulfuric acid concentration.

To recover metals from leach liquors a tin and indium precipitations are necessary. Tin precipitation is performed by using polyamine and indium precipitation is about getting an insoluble indium salt that is insoluble in water (like indium carbonate).

The precipitation tests have not been carried out as it is possible to have high precipitation yields only by recirculating the leaching solution for numerous steps until reaching high concentrations of the two elements under consideration. The latter will be studied in detail on the pilot plant (D5.4).

3.5 Liquid crystal displays – printed circuit boards (EuroLCDs)

Several leaching tests were performed to evaluate the recovery efficiency of Au, Ag, Pd, Cu and Sn through Gold-Rec1 and Gold-Rec2 processes on the AF81 components. The Gold-Rec1 process was performed for electronic board powders (after grinding) while Gold-Rec2 was used for the different devices (for example Blue Back Panel and Large Black Connection Devices).

3.5.1 PCBs powders leaching

The conditions of the Gold-Rec1 test carried out on the powders are the following:

- Solid concentration 15% wt./vol.
- Mixing 200 rpm
- H₂O₂ 20% vol.
- H₂SO₄ 10% vol.
- Thiourea 20 g/L
- Ferric sulphate 22.46 g/L

The test carried out was structured on 4 steps. The first three 90 min steps for the leaching of the base metals and the third 60 min step for the leaching of gold and silver by thiourea. Table 31 shows the results obtained in terms of recovery yields.

| Element | Concentration |
|----------|---------------|
| Au [ppm] | 73.37 |
| Ag [ppm] | 548.43 |
| Pd [ppm] | 38.66 |
| Cu (%) | 10.01% |
| Sn (%) | 2.50% |

Table 30. Characterization of PCBs powders

Table 31. Extraction yields for different AF81 powders

| Extraction yields | Step I | Step II | Step III | Step IV | Total |
|-------------------|--------|---------|----------|---------|-------|
| Au | 0.6% | 1.0% | 0.5% | 24.3% | 24.3% |
| Ag | 4.3% | 3.3% | 2.7% | 52.3% | 52.3% |
| Pd | 57.3% | 14.0% | 5.5% | 8.1% | 8.1% |
| Cu | 10.0% | 53.5% | 20.2% | 0.8% | 83.7% |
| Sn | 27.9% | 6.9% | 8.1% | 0.3% | 42.9% |

The fact of having obtained such low extraction yields of precious metals certainly depends on the presence of some components that hinder leaching (for example, components with a high copper content). In order to have higher yields it is necessary to remove these components before proceeding with the grinding. In this sense, the percentage of copper or other substances (mainly organic) which have a negative effect on the yield is reduced. For example, it has been seen that inductances must be removed. In this way it is possible to minimize the amount of metals that remain in the matrix.

3.5.2 Blue Back Panel leaching

The conditions of the Gold-Rec2 test carried out on the Blue Back Panel are the following:

- Solid concentration 15% wt./vol.
- Mixing 200 rpm
- H₂O₂ 20% vol.
- C₂H₄O₂ 10% vol.
- HCl 3.5 M

The test carried out was structured on 2 steps of 3 hours each. Table 33 Table 31shows the results obtained in terms of recovery yields.

Table 32. Characterization of Blue Back Panel

| Element Concentra | |
|-------------------|--------|
| Au [ppm] | 174.55 |
| Ag [ppm] | 204.62 |
| Pd [ppm] | 742.00 |
| Cu (%) | 28.99% |
| Sn (%) | 1.45% |

Table 33. Extraction yields for Blue Back Panel

| Extraction yields | Step I | Step II | Total |
|-------------------|--------|---------|-------|
| Au | 15.4% | 67.9% | 83.4% |
| Ag | 60.8% | 11.4% | 72.2% |
| Pd | 52.2% | 45.1% | 97.3% |
| Cu | 85.5% | 13.9% | 99.5% |
| Sn | 99.2% | 0.4% | 99.6% |

3.5.3 Large Back Panel leaching

The conditions of the tests carried out on the Large Black Connection Devices are the following:

- Solid concentration 15% wt./vol.
- Mixing 200 rpm
- H₂O₂ 20% vol.
- C₂H₄O₂ 10% vol.
- HCl 3.5 M

The test carried out was structured on 2 steps of 3 hours each. Table 35 Table 31shows the results obtained in terms of recovery yields.

Table 34. Characterization of Large Black Connection Devices

| Element | Concentration |
|----------|---------------|
| Au [ppm] | 731.92 |
| Ag [ppm] | 544.12 |
| Pd [ppm] | 54.89 |
| Cu (%) | 74.00% |
| Sn (%) | 3.92% |

Table 35. Extraction yields for Large Black Connection Devices

| Extraction yields | Step I | Step II | Total |
|-------------------|--------|---------|--------|
| Au | 0.4% | 8.1% | 8.6% |
| Ag | 42.0% | 31.2% | 73.2% |
| Pd | 68.7% | 31.3% | 100.0% |
| Cu | 64.2% | 35.7% | 99.9% |
| Sn | 0.0% | 98.0% | 98.0% |

The gold recovery yield is very low. This may be because the gold is less exposed to acid and therefore an additional stage of treatment may be required. Unfortunately, the material is no longer available to be able to proceed with further experimental tests.

All processes were carried out using new reagents for each step. To reduce consumption, a cross-leaching configuration will be carried out on a pilot scale. The obtained leaching yields are relatively low if compared with the yields obtained with the same process on materials very similar to those used. In this regard, the studied process is to be studied in more detail for its optimization.

4. Process analysis: simulation and cost analysis

4.1 Flexible electronics (TNO)

Batch leach tests were conducted by mixing the samples material with Dimethylformamide (DMF leaching) in a glass vessel, with agitation for 0.5 and 24 h respectively, and separating the leachate from solid material by centrifugation. Spent leachate (spent DMF) was subjected to evaporation treatment in order to evaluate the effectiveness of DMF recycling. Instead, solid material was subjected to subsequent Thiourea Leaching.



Figure 18. Simplified process scheme for flexible electronics 1

On the basis of the experimental tests carried out on a laboratory scale (chapter 3.1), the material balances were made. The recovery yield of Ag is about 97%. Thanks to the material balance it was possible to define the OPEX of the process both for a scenario without DMF recirculation, and for a scenario with the recirculation of about 70% of this reagent. The tables below report the results obtained.

| INPUT | | OUTPUT | | |
|-----------------------|---------|-------------------------------|---------|--|
| Description | kg | Description | kg | |
| Solid (Flex Circuits) | 1 000.0 | Solid (spent plastic) | 415.2 | |
| DMF | 7 802.6 | Silver powder | 3.12 | |
| Water | 3 693.3 | Plastic after evaporation | 613.5 | |
| Thiourea | 70.9 | Solid waste after Ag leaching | 81.2 | |
| Ferric sulfate | 78.1 | Wastewater | 3 836.0 | |
| Sulfuric acid, 50 % | 106.7 | Spent DMF non-recyclable | 2 340.8 | |

Table 36. Mass balance for the treatment of a ton of Flex Circuits

| Chemicals | Mass, kg | Unit cost, €/kg | Cost, € |
|------------------------|----------|-----------------|-----------------|
| DMF | 7 802.6 | 1.2 | 9 363.1 |
| Thiourea | 70.9 | 1.00 | 70.90 |
| Ferric sulphate | 78.1 | 0.30 | 23.43 |
| Sulfuric acid, 50 % | 106.7 | 0.13 | 13.8 |
| Water | 3 693.3 | 0.0015 | 5.54 |
| | | | Total 9 476.7 |
| OPEX | | | |
| items | | | cost, € |
| chemicals | | | 9 476.7 |
| wastewater to disposal | 100 | €/m³ | 383.6 |
| solid disposal | | | |
| silver powder | 0.7 | 2 €/g | 2 246.4 |
| | | | Total - 7 613.9 |

Table 38. Chemical consumption and costs for the recycling of silver from a ton of Flex Circuits

| Chemicals | Mass, kg | Unit cost, €/kg | Cost, € | |
|-------------------------------|----------|-----------------|----------------------|--|
| Considering 70% DMF recycling | 2340.8 | 1.20 | 2808.9 | |
| Thiourea | 70.9 | 1.00 | 70.90 | |
| Ferric sulphate | 78.1 | 0.30 | 23.43 | |
| Sulfuric acid, 50 % | 106.7 | 0.13 | 13.8 | |
| Water | 3693.3 | 0.0015 | 5.54 | |
| | | | Total 2 922.6 | |
| OPEX | | | | |
| items | | | cost,€ | |
| chemicals | | | 2 922.6 | |
| wastewater to disposal | 100 €/m³ | | 383.6 | |
| solid disposal | | | recycling evaluation | |
| silver powder | 0.72 € | E/g | 2 246.4 | |
| | | | Total - 1 059.8 | |

The residual solid was not analyzed in detail but consists of spent plastic. The wastewater was characterized with semi-quantitative analysis by ICP-OES. The wastewater contains thiourea and related degradation compounds, with different metals. The main results obtained are summarized in the table below.

Table 39. Semi-quantitative analysis of wastewater (ICP-OES analysis)

| Metal | Concentration [mg/L] |
|-------|----------------------|
| Fe | 1000 |

| Cu | 60 |
|----|----|
| Mn | 10 |

For the moment, the price of the metal with a purity of 100% has been considered in the balance sheet. No other metal impurities were detected from the analyses on the silver dust obtained. Impurities are organic materials from chemicals and anode material. Probably, after refining, the purity of silver approaches 100%. Due to the small quantities obtained on the lab scale, this aspect has to be evaluated on a pilot scale.

4.2 In-mold electronics (TNO)

The proposed process for the treatment of this material consists of 2 leaching steps in crossleaching configuration with make-up of chemicals in the second step. At the end of each of the two steps, the solid phase is separated from the liquid phase by means of a filtering system. From the second filtration, the resulting solution is sent to an electrolysis cell. From here comes out a liquid stream with about 25 mg/L of Ag which is recirculated at the head of the process, and a solid stream made up of silver powder.



Figure 19. Flowsheet for the recycling of silver from thermoformed samples

On the basis of the experimental tests carried out on a laboratory scale (chapter 3.2), the material balances were made. The recovery yield of Ag is about 90%. Thanks to the material balance it was possible to define the OPEX of the process. Table 40 reports the material balance of the process while in Table 41 is shown the chemicals costs.

Table 42 summarizes the OPEX of the process.

Table 40. Mass balance for the treatment of a ton of thermoformed samples

| INPUT | | OUTPUT | |
|------------------------------|--------|------------------------------|--------|
| description | kg | description | kg |
| solid (thermoformed samples) | 1000.0 | solid (thermoformed samples) | 991.6 |
| water | 3143.5 | silver powder | 4.4 |
| thiourea | 151.7 | wastewater | 3908.0 |
| ferric sulphate | 343.1 | | |
| sulfuric acid, 50 % | 265.7 | | |
| Total | 4904.0 | | 4904.0 |

| CHEMICALS | MASS [kg] | UNIT COST [€/kg] | COST [€] |
|---------------------|-----------|------------------|----------------|
| thiourea | 151.7 | 1.00 | 151.70 |
| ferric sulphate | 343.1 | 0.30 | 102.93 |
| sulfuric acid, 50 % | 265.7 | 0.13 | 34.54 |
| water | 3143.5 | 0.0015 | 4.72 |
| | | | Total 293.89 € |

Table 41. Chemical consumption and costs for the recycling of a ton of thermoformed samples

Table 42. Operating costs for the recycling of a ton of thermoformed samples

| ITEMS | | COST [€] |
|------------------------|--|-----------|
| Chemicals | | - 293.89 |
| wastewater to disposal | 100 €/m³ | - 379.50 |
| solid disposal | | |
| onorgy consumption | electrowinning (3 kWh/kg) - 0.20 €/kWh | - 2.62 |
| energy consumption | agitators | |
| silver powder | 0.72 €/g | + 3146.40 |
| Total | | + 2470,39 |

The wastewater was characterized with semi-quantitative analysis by ICP-OES. The wastewater contains thiourea and related degradation compounds, with different metals summarized in the table below.

Table 43. Semi-quantitative analysis of wastewater

| Metal | Concentration [mg/L] | | |
|-------|----------------------|--|--|
| Fe | 1000 | | |
| Cu | 50 | | |
| Mn | 20 | | |

Currently, the price of the metal with a purity of 100% has been considered in the balance sheet. No other metal impurities were detected from the analyzes on the silver dust obtained. Impurities are organic materials from chemicals and anode material. Probably, after refining, the purity of silver approaches 100%. Due to the small quantities obtained on the lab scale, this aspect has to be evaluated on a pilot scale.

4.3 Electronic car components (SEAT

4.3.1 PCBs powders leaching



Figure 20. Simulation of Gold-Rec1 process for Ibiza IV powders treatment

On the basis of the experimental tests carried out on a laboratory scale (chapter 3.3.1), the material balances were made. The recovery yield of all elements is reported below:

- Gold: 62%
- Silver: 21%
- Copper: 98%
- Tin: 90%

Thanks to the material balance it was possible to define the OPEX of the process.

Table 44. Material balance for of Gold-Rec1 process for Ibiza IV powders treatment

| INPUT | | OUTPUT | |
|----------------------------|------|----------------|--------|
| Solid [kg] | 1000 | Solid [kg] | 766 |
| STEP 1 | | | |
| Hydrogen peroxide, 30% [L] | 1333 | Gold [kg] | 0.032 |
| Sulfuric Acid, 96% [L] | 667 | Silver[kg] | 0.136 |
| Water [L] | 4667 | Palladium [kg] | - |
| Washing Water [L] | 2000 | Copper [kg] | 160.75 |
| STEP 2 | | Tin Oxide [kg] | 15.43 |
| Hydrogen peroxide, 30% [L] | 1333 | Wastewater [L] | 21802 |
| Sulfuric Acid, 96% [L] | 667 | | |
| Water [L] | 4667 | | |
| Washing Water [L] | 2000 | | |
| STEP 3 | | | |
| Sulfuric Acid, 96% [L] | 87 | | |
| Thiourea [kg] | 154 | | |
| Ferric sulphate [kg] | 173 | | |
| Water [L] | 7636 | | |
| Washing Water [L] | 2000 | | |

Table 45. Operating costs for the recycling of a ton of dashboard electronic boards powdersfrom Ibiza IV without recycling of water

| Chemicals | Mass [kg] | Unit Cost [€/kg] | | Cost [€] |
|--------------------------|-------------------------|---------------------|---|-----------|
| Hydrogen peroxide, 35% | 2537 | 0.40€ | | 1,014.86€ |
| Sulfuric acid, 50% | 5016 | 0.13€ | | 652.10€ |
| Thiourea | 154 | 1.00€ | | 154.46€ |
| Ferric sulphate | 173 | 0.30€ | | 51.93€ |
| Water | 21228 | 0.0015€ | | 31.84€ |
| Total | · · · · · | | | 890.34€ |
| OPEX (1000 kg/h sample) | (No recycling of water) | | | |
| Chemicals | | | - | 890.34 € |
| Wastewater (to disposal) | 150 €/m³ | | - | 3,270.30€ |
| Solid (to disposal) | 100 €/ton | | - | 76.60€ |
| Energy consumption | Agitators (6x20kW) | | - | 52.55€ |
| Precipitation section | Electro | winning (3x3kWh/kg) | - | 169.42€ |

| | Chemicals | - | 32.17€ |
|-----------|------------------|---|------------|
| Total | | - | 4,491.38€ |
| Products | Unit Cost [€/kg] | | |
| Gold | 53,696.49 € | | 1,718.29€ |
| Silver | 621.00€ | | 84.58€ |
| Palladium | 63,272.67 € | | - € |
| Copper | 3.50€ | | 562.63€ |
| Tin Oxide | 50.00 € | | 771.50€ |
| REVENUES | | - | 1,354.39 € |

Table 46. Operating costs for the recycling of a ton of dashboard electronic boards powders from Ibiza IV with recycling of 60% of water

| OPEX (1000 kg/h sample) | (Recycling of 60% of water) | | | |
|--------------------------|-----------------------------|---|------------|--|
| Chemicals | | - | 890.34 € | |
| Wastewater (to disposal) | 150 €/m³ | - | 1,308.12 € | |
| Solid (to disposal) | 100 €/ton | - | 76.60€ | |
| Energy consumption | Agitators (6x20kW) | - | 52.55€ | |
| Draginitation contian | Electrowinning (3x3kWh/kg) | - | 169.42€ | |
| Precipitation section | Chemicals | - | 32.17€ | |
| Total | | - | 2,529.20€ | |
| Products | Unit Cost [€/kg] | | | |
| Gold | 53,696.49 € | | 1,718.29€ | |
| Silver | 621.00€ | | 84.58€ | |
| Palladium | 63,272.67 € | | - € | |
| Copper | 3.50€ | | 562.63€ | |
| Tin Oxide | 50.00 € | | 771.50€ | |
| REVENUES | | | 607.79 € | |

The residual solid was characterized respectively with elemental CHNS analysis and with semiquantitative analysis by ICP-OES. The residual solid mainly contains plastics, glass fibers, carbon residues and unrecovered metal traces. The wastewaters were characterized with semiquantitative analysis by ICP-OES. The main results obtained are summarized in the tables below.

Table 47. Elemental CHNS analysis results of the residual solid

| Element | Results (wt%) |
|----------|---------------|
| Carbon | 17.03 |
| Hydrogen | 1.02 |
| Nitrogen | 0.56 |
| Sulfur | 0.36 |

Table 48. Semi-quantitative results of residual solid

| Fe | 50 |
|----|-----|
| Ti | 50 |
| Sn | 30 |
| Ni | 20 |
| Zr | <10 |
| Zn | <5 |

Table 49. Wastewater characterization

| Wastewater 1 | acid, sulfuric solution, mainly containing zinc, nickel, aluminum, iron |
|--------------|--|
| Wastewater 2 | weakly acidic solution with thiourea, urea, cyanamide, sulfur, iron and zinc |

Table 50. Semi-quantitative results of wastewaters

| | Metal | Concentration [mg/L] |
|--------------|------------|----------------------|
| Wastewater 1 | Fe | 500 |
| | Ni | 100 |
| | Sn, Ti, Zn | <20 |
| | Fe | 1000 |
| Wastewater 2 | Cu | 20 |
| | Mn, Ni | <20 |

4.4 Liquid crystal displays (EuroLCDs)

The proposed process for the treatment of ITO glasses consists of two steps: pre-treatment and leaching. In the first step, the feeding stream is washed with water to remove the surface coating layer. After washing, filtration takes place to separate the wastewater from the solid which is sent to the leaching step. Leaching takes place at 60 °C using very diluted sulfuric acid. A new filter system is inserted downstream of the leaching system to separate the residual solid phase from the leach liquor.



Figure 21. Pre-treatment and leaching process scheme

The precipitation of the tin is carried out by means of polyamine. The precipitation tests have not been carried out as it is possible to have high precipitation yields only by recirculating the leaching solution for numerous steps until reaching high concentrations of the two elements under consideration. The latter will be studied in detail on the pilot plan

4.5 Liquid crystal displays - printed circuit boards (EuroLCDs)

4.5.1 Blue Back Panel



Figure 22. Simulation of Gold-Rec2 process for Blue Back Panel treatment



On the basis of the experimental tests carried out on a laboratory scale (chapter 3.5.1), the material balances were made. The recovery yield of all elements is reported below:

- Gold: 84%
- Silver: 73%
- Palladium: 98%
- Copper: 99.5%
- Tin: 99.5%

Thanks to the material balance it was possible to define the OPEX of the process.

Table 51. Material balance for of Gold-Rec2 process for Blue Back Panel treatment

| INPUT | | OUTPUT | |
|----------------------------|------|----------------------|-------|
| Solid [kg] | 1000 | Solid [kg] (plastic) | 696 |
| STEP 1 | | | |
| Hydrogen peroxide, 30% [L] | 1333 | Gold [kg] | 0.137 |
| Hydrochloric Acid, 37% [L] | 1945 | Silver Chloride [kg] | 0.185 |
| Acetic Acid, 99.9% [L] | 667 | Palladium [kg] | 0.678 |
| Water [L] | 2722 | Copper [kg] | 271 |
| Washing Water [L] | 2000 | Tin [kg] | 506 |
| STEP 2 | · | Wastewater [L] | 17572 |
| Hydrogen peroxide, 30% [L] | 1333 | | |
| Hydrochloric Acid, 37% [L] | 1945 | | |
| Acetic Acid, 99.9% [L] | 667 | | |
| Water [L] | 2722 | | |
| Washing Water [L] | 2000 | | |

Table 52. Operating costs for the recycling of a ton of Blue Back Panel without recycling of water

| Chemicals | Mass [kg] | Unit Cost [€/kg] | Cost [€] | |
|--------------------------|-----------|----------------------|----------|-----------|
| Hydrogen peroxide, 35% | 2537 | 0.40€ | | 1,014.86€ |
| Hydrochloric Acid, 32.5% | 5313 | 0.18€ | | 956.38€ |
| Acetic Acid, 80% | 1748 | 0.60€ | | 1,048.95€ |
| Water | 8951 | 0.0015€ | | 13.43€ |
| Total | | | | 2,018.76€ |
| OPEX (1000 kg/h sample) | | (No Recycling of wat | er) | |
| Chemicals | | | - | 2,018.76€ |
| Wastewater (to disposal) | | 150 €/m³ | - | 2,635.80€ |





| Solid (to disposal) | 100 €/ton | - | 69.60€ |
|-----------------------|----------------------------------|---|-------------|
| Energy consumption | Cooling Water (Ag precipitation) | - | 52.55€ |
| | Agitators (6x20kW) | - | 56.00€ |
| Precipitation section | Chemicals | - | 5,766.55€ |
| Total | | - | 10,599.26€ |
| Products | Unit Cost [€/kg] | | |
| Gold | 53,696.49 € | | 7,356.42€ |
| Silver Chloride | 50.45 € | | 9.33€ |
| Palladium | 63,272.67 € | | 42,898.87€ |
| Copper | 3.50€ | | 948.50€ |
| Tin | 28.26€ | | 14,286.00€ |
| REVENUES | | | 54,899.86 € |

The residual solid and the wastewater were characterized. The residual solid mainly contains plastics. The wastewater contains hydrochloric acid with different metals summarizes in the table below.

Table 53. Composition of wastewater (to wastewater treatment) in terms of metals

| Component | | Concentration |
|-------------------|------|---------------|
| CuCl ₂ | mg/L | 842.2 |
| PdCl ₂ | mg/L | 1.6 |
| SnCl ₂ | mg/L | 1196 |
| ZnCl ₂ | g/L | 42.1 |





5. Conclusions

Numerous laboratory-scale analyses were performed to characterize the different materials provided by the project partners. Using the results of these analyses, a sustainable recovery process that could guarantee high extraction yields was studied for each material. A technical and economic feasibility analysis was performed for the different processes studied and developed.

The main results obtained for the various components of interest within the Project are reported below: flexible electronics (2 types), car dashboard, printed circuit boards of LCD and ITO glass of LCD.

Flexible electronics (type 1)

- From the characterization of the material, an average silver concentration of 0.31 wt. % was determined, considering the full weight of the sample. The silver present in this type of material was embedded so it is required a pre-treatment to dissolve the plastic and facilitate access to the metal parts.
- The flexible electronics were subjected to two successive leaching steps (Gold-Rec1 modified): DMF treatment to remove the plastic layer and thiourea leaching to extract silver.
- A silver extraction yield of approximately 97% was achieved.
- Il processo proposto è stato studiato considerando un ricircolo di circa il 70% di DMF.

Flexible electronics/IME (type 2)

- From the characterization of the material, an average silver concentration between 0.36-0.63 wt. % was determined, considering the full weight of the sample. The silver present in this type of material was directly accessible (on the surface).
- The samples were subjected to different experimental tests to study the recovering of silver from the polycarbonate-based IME: thiourea leaching and thiourea leaching without oxidant agent. The first (2 steps) allowed a recovery over 90% while the second showed that no significant Ag dissolution occurred (recovery yield < 6%) performing thiourea leaching without the oxidant agent (Fe³⁺).
- A recovery process using electrowinning has been studied and it has been seen that it is possible to recover about 95% of Ag if one works for 2 hours with a voltage 1.2 V and current density 43 A/m2.

It has been seen that it is possible to optimize the process through a cross-leaching scheme. Indeed, it is possible to recycle the solution in 3 batches before disposing of as wastewater.



Car dashboard of SEAT

- From the characterization of the material (for all three car models), the following composition of the device was determined: 76.3% plastic (with traces of glass), 23.56% electronic board and 0.14% aluminum (screws) (the results refer to the Leon II model but are similar for all three models). The electronic board has been characterized in detail in terms of metals present and in particular of Au, Ag, Pd, Cu and Sn; in addition to the metallic fraction is also composed to plastics, fiber glass and epoxy resin.
- The Printed Circuit Boards (PCBs) powders obtained by grinding were subjected to the Gold-Rec1 process. PCBs powders leaching has recorded relatively low recovery yields and is still being optimized today.
- It was seen that using the Gold-Rec1 process on the board powders without electronic components becomes sustainable only if there is recirculation of the water used in the process (at least 60% of the water used).

Printed circuit boards of LCD

- All the components on the board were detached, by heating and manual removal, in order to chemically characterize each type. The composition of each of the components and of the board itself was determined.
- The board has been milled and subjected to the Gold-Rec1 process while the components richer in precious metals (back panels) have been subjected to the Gold-Rec2 process. Also, for this material a low extraction yield of precious metals has been obtained which must be optimized by eliminating other components with a high copper content.

For back panels the situation is different depending on the material being treated. In this case it could be the plastic material that influences the yields.

• For the powders and back panels from the PCBs of liquid crystal displays, it has been seen that the process is highly cost-effective. Suppose only the connection peripherals are considered. In that case, the revenue obtained is high and would allow the whole board to be treated while continuing to have an economically viable process.

ITO glass of LCD

- From the characterization of the material, the following composition of the device was determined: 60-70 g/t In and 15-25 g/t Sn.
- A series of experimental tests was carried out to understand the behavior of this material in different situations. Washing using acetone and water has used us pre-treatment for the removal of the protective layer covering the metals. When the pre-treatment was used, the leaching step (sulfuric acid leaching) allows recovery about 99% of In and 53% of Sn after 1h. Without the pre-treatment the leaching step allows recovery about 80.6% of In and 65% of Sn after 1h.
- To optimize the process, a factorial plan was created which made it possible to identify the best recovery conditions for In (of greatest interest), with almost total recovery (T=60 °C; H2SO4 concentration= 1 mol/L; pulp density = 15 % wt. /v); under these conditions the recovery of Sn was about 50%.





• The indium and tin recovery processes are not economically feasible when treating ITO glasses when taken individually. To be feasible, the process of recovering these elements must be integrated into a process of recovering the other components of this material.

However, it should be remembered that all the tests carried out were conducted on materials supplied mainly by manufacturers and not disposers. On the pilot plant, the different processes studied will be evaluated, with all the background knowledge gained on these materials, also for materials from disposers (i.e. POLLINI, ILLSA etc.). Prior to pilot-scale experimentation, appropriate laboratory experimental verifications will be carried out on the materials from the disposers.





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| ICP-OES | Inductively Coupled Plasma – Optical Emission Spectroscopy |
|---------|--|
| XRF | X-ray fluorescence spectroscopy |
| XRD | X-ray diffraction |
| PET | Polyethylene terephthalate |
| TPU | Thermoplastic polyurethane |
| IME | In-Mold Electronics |
| PCBs | Printed Circuit Boards |
| LCD | Liquid Crystal Displays |
| ITO | Indium-tin oxide |
| DMF | Dimethylformamide |

Abbreviations





Appendix A: Arduino

A characterization study was carried out on a very widespread and standard board at a global level, namely the Arduino board. This study made it possible to define the main elements present in general in an electronic board and to define the source of each in terms of electronic components.

In order to carry out this analysis, we started with a removal of all the components present on the board and their identification based on the function performed. Subsequently, each of the removed elements was subjected to chemical attack (CA) by means of aqua regia or different acids.

The resulting solutions were analyzed by ICP-OES to determine the metal content.

| Photo | Name | Weight [g] | (Wt.%) | Elements reported by the qualitative analysis | Comp | osition | Method |
|-------|-----------|---------------|---------|---|----------|---------|----------------------|
| | | | | | CA [g] | 0.0031 | Aqua regia digestion |
| | | | | | Cu (%) | 24.47 | |
| | | | | | Sn (%) | 8.08 | |
| | | 0.0031 | 0.006% | Ag, Al, Au, B, Cu, Fe, Ga, Ni, Pd, Sn, Zn | Ni (%) | 4.97 | |
| | TX-LX-L- | | | | AI (%) | 2.11 | |
| | Power Led | | | | Zn (%) | 0.34 | |
| | | | | | Fe (%) | 0.19 | |
| | | | | | Ag [ppm] | 2096.77 | |
| | | | | | Au [ppm] | 1774.19 | |
| | | | | | Pd [ppm] | 161.29 | |
| | | | 0.054% | Ag, Al, Au, B, Cu, Ni, Pd, Sn, Zn | CA [g] | 0.0282 | Aqua regia digestion |
| | | | | | Cu (%) | 38.41 | |
| | | | | | Sn (%) | 9.38 | |
| | | | | | Ni (%) | 0.67 | |
| | PolyFuse | 0.0281 | | | AI (%) | 0.49 | |
| | | | | | Zn (%) | 0.24 | |
| 计时间接入 | | | | | Ag [ppm] | 2801.42 | |
| | | | | | Au [ppm] | 726.95 | |
| | | | | | Pd [ppm] | 53.19 | |
| | M7 Diode | 0.0646 | 0.125% | Ag, Au, Cu, Pb, | CA [g] | 0.0644 | Aqua regia digestion |
| | | | 0.123/0 | Pd, Sn, Zn | Cu (%) | 33.95 | |

Table 1.A. Results of components characterization





| | | | | | Sn (%) | 4.26 | |
|----------------------|----------------------|--------|---------|--|----------|---------|---|
| | | | | | Zn (%) | 0.21 | |
| | | | | | Ag [ppm] | 1374.22 | |
| | | | | | Pd [ppm] | 46.58 | |
| | | | | | CA [g] | 0.129 | They were cut and |
| | | | | | Cu (%) | 42.80 | then submitted to aqua regia digestion |
| | | | | | Sn (%) | 2.96 | |
| | Voltage Regulator | 0.1292 | 0.250% | Ag, Au, B, Co, Cu, Fe, Pd, Pt, | Zn (%) | 0.29 | |
| | Regulator | | | Sn, Zn | Fe (%) | 0.02 | |
| | | | | | Ag [ppm] | 3573.64 | |
| | | | | | Pd [ppm] | 58.14 | |
| | | | | | CA [g] | 0.1972 | Aqua regia digestion |
| | | | | | Cu (%) | 13.85 | |
| | Reset | | 0.381% | | Zn (%) | 7.12 | |
| | | 0.1965 | | Ag, Al, Au, B, Cu, Fe, Mn, | Sn (%) | 0.87 | |
| | | | | Pd, Pt, Rb, Sn, Zn | Fe (%) | 0.60 | |
| | | | | | Al [ppm] | 519.78 | |
| | | | | | Ag [ppm] | 403.14 | |
| | | | | | Pd [ppm] | 17.75 | |
| | | | | | CA [g] | 0.5028 | Aqua regia digestion |
| | 16 MHz | 0 5022 | 0.975% | Ag, Au, Co, Cu, Fe, Mn, Ni, Pd, Rb, Sn, Zn | Fe (%) | 14.21 | |
| | | | | | Cu (%) | 9.62 | |
| 1. 12 Link police 1 | | | | | Zn (%) | 5.36 | |
| | Oscillator | 0.5055 | | | Sn (%) | 0.05 | |
| unity as I The State | | | | | Ni (%) | 0.01 | |
| Tu il se il Matte | | | | | Ag [ppm] | 904.93 | |
| | | | | | Pd [ppm] | 1.99 | |
| | | | | | CA [g] | 0.5338 | They were cut and |
| | | | | | Fe (%) | 59.50 | aqua regia digestion |
| | | | | | AI (%) | 37.76 | |
| | Capacitors | 0.5409 | 1.048% | Ag, Al, Au, B, Cu, Fe, Pd, Pt | Cu (%) | 0.41 | |
| | Sapacitors | 0.0105 | 2.010/0 | Rb, Sn, Zn | Sn (%) | 0.27 | |
| | | | | | Zn (%) | 0.01 | |
| | | | | | Ag [ppm] | 59.01 | |
| | | | | | Pd [ppm] | 0.94 | |
| | ICC | 0.6288 | 1.219% | | CA [g] | 0.626 | |
| | | | | | | | |





| | | | | | Cu (%) | 28.75 | |
|---|------------------|--------|---------|---|-------------|--------|-------------------------------------|
| | | | | | Sn (%) | 3.19 | |
| 外别的教育的 的"小人" | | | | | Fe (%) | 1.67 | |
| Communication and Communication | | | | Ag, Au, Co, Cu, Fe, Ni, P, Pd, | Zn (%) | 0.17 | They were cut and then submitted to |
| Real Real Property of the second s | | | | Sn, Zn | Ag [ppm] | 638.57 | aqua regia digestion |
| | | | | | Au [ppm] | 190.77 | |
| | | | | | Pd [ppm] | 33.52 | |
| | | | | | Plastic [g] | 0.190 | Aqua regia digestion |
| | | | | | CA [g] | 0.607 | |
| | | | | Ag, Au, B, Cu, Ni, P, Pd, Sb, Sn, Zn | Cu (%) | 58.40 | |
| | | | | | Zn (%) | 28.99 | |
| | ICSP | 0.7997 | 1.550% | | Sn (%) | 12.41 | |
| | | | | | Ni (%) | 1.02 | |
| | | | | | Ag [ppm] | 975.29 | |
| | | | | | Au [ppm] | 62.60 | |
| | | | | | Pd [ppm] | 59.31 | |
| | | | | | Plastic [g] | 0.685 | Agua regia digestion |
| | | 1.3288 | 2.575% | Ag, Au, Cu, Fe, Mn, Ni, P, Pd, Pt, Rb, Sn, Zn | CA [g] | 0.643 | |
| | DC Power Jack | | | | Cu (%) | 48.57 | |
| | | | | | Zn (%) | 25.53 | |
| | | | | | Fe (%) | 19.07 | |
| | | | | | Sn (%) | 7.03 | |
| | | | | | Ni (%) | 0.24 | |
| | | | | | Ag [nnm] | 810.89 | |
| | | | | | Pd [ppm] | 45 14 | |
| | | | | | Plastic [g] | 1 531 | They were broken |
| | | | | | | 1 875 | and then submitted |
| | | | | | | 63 11 | digestion |
| | | | | | Zn (%) | 25.81 | |
| | USB-B | 3 406 | 6 601% | Ag, Au, Cu, Ni, | Sn (%) | 4.82 | |
| | Port | 3.400 | 0.00176 | Pd, Rb, Sn, Zn | NI: (%) | 4.02 | |
| The second | | | | | NI (70) | 402.02 | |
| | | | | | | 402.93 | |
| | | | | | | 49.87 | |
| | | | | | Au [ppm] | 4.53 | |
| | External Pin | 7.9289 | 15.366% | Ag, Au, Cu, Ni, Pd, Rb, Sn, Zn | | 5.505 | Aqua regia digestion |
| | | | | ·,, etty Ett | CA [g] | 2.423 | |





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| Cover 15.23 29.515% - CA [g] 15.230 Image: Cover 15.23 29.515% - CA [g] - - Image: Cover 15.23 29.515% - CA [g] 18.377 - Image: Cover Image: Cover Image: Cover Image: Cover Image: Cover - - Image: Cover Image: Cover Image: Cover Image: Cover - - - Image: Cover Image: Cover Image: Cover Image: Cover Image: Cover - - Image: Cover Image: Cover Image: Cover Image: Cover - - Image: Cover Image: Cover Image: Cover Image: Cover - - - Image: Cover Image: Cover Image: Cover Image: Cover Image: Cover - - - Image: Cover Image: Cover Image: Cover Image: Cover Image: Cover - - - Image: Cover Image: Cover Image: Cov |
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| Board 20.251 39.246% Ag, B, Ba, Bi, Ca, Cu, Fe, Mg, Mn, Na, Ni, Pd, Si, Sn, Ti, Zn CA [g] 18.377 It was cut and ther submitted to aqua regia digestion Image: Campa digestion 30.246% Ag, B, Ba, Bi, Ca, Cu, Fe, Mg, Mn, Na, Ni, Pd, Si, Sn, Ti, Zn Sn (%) 3.36 Image: Campa digestion 350.33 Ti [ppm] 350.33 |
| Board 20.251 39.246% Ag, B, Ba, Bi, Ca, Cu, Fe, Mg, Mn, Na, Ti, Zn Cu (%) 15.09 regia digestion Ti [ppm] 350.33 Ti [ppm] 350.33 Ti [ppm] 86.03 |
| Board 20.251 Ag, B, Ba, Bi, Ca, Cu, Fe, Mg, Mn, Na, Ni, Pd, Si, Sn, Ti, Zn Sn (%) 3.36 Image: Constraint of the second s |
| Board 20.251 39.246% Ca, Cu, Fe, Mg, Mn, Na, Ni, Pd, Si, Sn, Ti, Zn Zn (%) 0.36 4g [ppm] 350.33 350.33 10 10 10 |
| Ni, Pd, Si, Sn, Ti, Zn Ag [ppm] 350.33 Ti [ppm] 86.03 |
| Ti [ppm] 86.03 |
| |
| Pd [ppm] 14.80 |
| Au [ppm] 2.39 |
| Ti (%) 15.72 They were broken then were submittee |
| Cu (%) 6.93 to 1 hour therma |
| Sn (%) 6.07 with KOH (two times |
| Ag (%) 1.33 the the sample was |
| Ceramic Multilayer 0.164 0.318% Cu, Dy, Fe, Zn (%) 0.40 0.40 0.00° C for 1 h for the |
| Capacitors |
| Au [ppm] 103.66 was submitted to nitric acid for Ag and Cu digestion and ther to aqua regia digestion for Au, Po and Ti detection. |
| Sn (%) 5.46 Aqua regia digestion |
| - Transistor 0.093 0.180% Mn Ni Ph Sn |
| Zn (%) 0.04 |
| Ag [ppm] 2032.26 |





| | | | | Au [ppm] | 580.65 | |
|-------|-----------|--------|------------------------------------|----------|---------|----------------------|
| | | | | Sn (%) | 8.31 | Aqua regia digestion |
| | | | | Cu (%) | 3.42 | |
| | | | Ag, Ba, Bi, Ca, | Ti (%) | 0.48 | |
| - Oth | ers 0.115 | 0.223% | Cu, Fe, Mn, Ni, Pb, Pd, Sn, Ti, | Zn (%) | 0.05 | |
| | | | Zn, Zr | Ag [ppm] | 1813.04 | |
| | | | | Pd [ppm] | 300.00 | |
| | | | | Au [ppm] | 52.17 | |



Figure 1.A. Arduino composition



Figure 2.A. Metal fraction composition





Appendix B: flexible electronics - XRF analysis



Figure 1.B. Map of performed XRF analyses for the characterization of sample A





| Ζ | Symbol | Element | Norm. Int. | Concentration | Abs. Error | |
|----|--------|--------------|------------|---------------|-------------|--|
| 12 | Mg | Magnesium | 0.0000 | < 0.0020 % | (0.0) % | |
| 13 | AI | Aluminum | 15.0925 | < 0.0020 % | (0.0) % | |
| 14 | Si | Silicon | 306.3534 | 0.1584 % | 0.0006 % | |
| 15 | P | Phosphorus | 0.0000 | < 0.00030 % | (0.0) % | |
| 16 | S | Sulfur | 1024.4259 | 0.09242 % | 0.00016 % | |
| 17 | CI | Chlorine | 7039.4736 | 0.3001 % | 0.0002 % | |
| 19 | ĸ | Potassium | 1309.8280 | 0.5606 % | 0.0007 % | |
| 20 | Ca | Calcium | 0.0000 | < 0.0010 % | (0.0) % | |
| 22 | Ti | Titanium | 30.9095 | 0.00357 % | 0.00005 % | |
| 23 | V | Vanadium | 5.7787 | 0.00034 % | 0.00002 % | |
| 24 | Cr | Chromium | 9.5832 | 0.00033 % | 0.00001 % | |
| 25 | Mn | Manganese | 3871.0944 | 0.1323 % | 0.0002 % | |
| 26 | Fe | Iron | 3820.3295 | 0.2194 % | 0.0003 % | |
| 27 | Co | Cobalt | 0.9651 | < 0.00030 % | (0.0) % | |
| 28 | Ni | Nickel | 27.1627 | 0.00066 % | 0.00001 % | |
| 29 | Cu | Copper | 131.2786 | 0.00261 % | 0.00002 % | |
| 30 | Zn | Zinc | 11.9189 | 0.00016 % | 0.00001 % | |
| 31 | Ga | Gallium | 4.4748 | 0.00005 % | 0.00001 % | |
| 32 | Ge | Germanium | 0.0000 | < 0.00005 % | (0.0) % | |
| 33 | As | Arsenic | 0.0000 | < 0.00005 % | (0.0) % | |
| 34 | Se | Selenium | 2.5214 | < 0.00005 % | (0.00001) % | |
| 35 | Br | Bromine | 4.0084 | < 0.00005 % | (0.00002) % | |
| 37 | Rb | Rubidium | 2.9093 | < 0.00005 % | (0.0) % | |
| 38 | Sr | Strontium | 18.6010 | < 0.00005 % | (0.0) % | |
| 39 | Y | Yttrium | 1.8379 | < 0.00005 % | (0.0) % | |
| 40 | Zr | Zirconium | 0.0000 | < 0.00010 % | (0.0) % | |
| 41 | Nb | Niobium | 0.0000 | < 0.00010 % | (0.0) % | |
| 42 | Mo | Molybdenum | 1.0329 | 0.00002 % | 0.00001 % | |
| 47 | Ag | Silver | 4304.2630 | 0.2938 % | 0.0003 % | |
| 48 | Cd | Cadmium | 12.6772 | 0.00050 % | 0.00001 % | |
| 50 | Sn | Tin | 0.0000 | < 0.00030 % | (0.0) % | |
| 51 | Sb | Antimony | 0.0000 | < 0.00030 % | (0.0) % | |
| 52 | Те | Tellurium | 2.5344 | < 0.00030 % | (0.0) % | |
| 53 | 1 | lodine | 0.0000 | < 0.00030 % | (0.0) % | |
| 55 | Cs | Cesium | 0.0000 | < 0.00040 % | (0.0) % | |
| 56 | Ba | Barium | 0.0000 | < 0.00020 % | (0.0) % | |
| 57 | La | Lanthanum | 0.0000 | < 0.00020 % | (0.0) % | |
| 58 | Ce | Cerium | 0.0000 | < 0.00020 % | (0.0) % | |
| 59 | Pr | Praseodymium | 2.1031 | 0.00034 % | 0.00006 % | |
| 60 | Nd | Neodymium | 3.9447 | 0.00053 % | 0.00006 % | |
| 72 | Hf | Hafnium | 4.3778 | 0.00008 % | 0.00001 % | |
| 73 | Та | Tantalum | 16.0473 | < 0.00010 % | (0.0) % | |
| 74 | W | Tungsten | 1.5193 | < 0.00010 % | (0.0) % | |
| 80 | Hg | Mercury | 2.6738 | < 0.00010 % | (0.00003) % | |
| 81 | TI | Thallium | 3.3434 | < 0.00010 % | (0.00003) % | |
| 82 | Pb | Lead | 3.8560 | 0.00006 % | 0.00001 % | |
| 83 | Bi | Bismuth | 0.0000 | < 0.00010 % | (0.0) % | |
| 90 | Th | Thorium | 3.4819 | < 0.00010 % | (0.00003) % | |
| 92 | U | Uranium | 2,5352 | < 0.00010 % | (0.0) % | |

Table 1.B. XRF-analysis on flexible electronic (Sample A, area 1)





Table 2.B. XRF-analysis on flexible electronic (Sample A, area 2)

| z | Symbol | Element | Norm. Int. | Concentration | Abs. Error | |
|----|--------|--------------|------------|---------------|-------------|--|
| 12 | Ma | Magnesium | 0.0000 | < 0.0020 % | (0.0) % | |
| 13 | AI | Aluminum | 73 6823 | < 0.0020 % | (0.0) % | |
| 14 | Si | Silicon | 913 0952 | 0.4782 % | 0.0008 % | |
| 15 | P | Phosphorus | 31.0425 | 0.00623 % | 0.00015 % | |
| 16 | S | Sulfur | 3264.5297 | 0.3101 % | 0.0003 % | |
| 17 | CI | Chlorine | 298.8645 | 0.01104 % | 0.00003 % | |
| 19 | ĸ | Potassium | 44.2475 | 0.01903 % | 0.00021 % | |
| 20 | Ca | Calcium | 49.7790 | 0.00063 % | 0.00001 % | |
| 22 | Ti | Titanium | 125.4881 | 0.01324 % | 0.00009 % | |
| 23 | V | Vanadium | 21.0388 | 0.00141 % | 0.00005 % | |
| 24 | Cr | Chromium | 31.4012 | 0.00111 % | 0.00003 % | |
| 25 | Mn | Manganese | 14116.5111 | 0.4539 % | 0.0003 % | |
| 26 | Fe | Iron | 12076.9126 | 0.6383 % | 0.0005 % | |
| 27 | Co | Cobalt | 2.4330 | < 0.00017 % | (0.0) % | |
| 28 | Ni | Nickel | 45.7436 | 0.00123 % | 0.00002 % | |
| 29 | Cu | Copper | 310.8789 | 0.00672 % | 0.00003 % | |
| 30 | Zn | Zinc | 22.7999 | 0.00034 % | 0.00001 % | |
| 31 | Ga | Gallium | 0.3439 | < 0.00005 % | (0.0) % | |
| 32 | Ge | Germanium | 0.0000 | < 0.00005 % | (0.0) % | |
| 33 | As | Arsenic | 1.9967 | 0.00002 % | 0.00001 % | |
| 34 | Se | Selenium | 2.5407 | 0.00002 % | 0.00001 % | |
| 35 | Br | Bromine | 4.4707 | < 0.00005 % | (0.00003) % | |
| 37 | Rb | Rubidium | 5.8103 | < 0.00005 % | (0.00002) % | |
| 38 | Sr | Strontium | 39.0812 | < 0.00005 % | (0.0) % | |
| 39 | Y | Yttrium | 0.0000 | < 0.00005 % | (0.0) % | |
| 40 | Zr | Zirconium | 0.2934 | < 0.00010 % | (0.0) % | |
| 41 | Nb | Niobium | 0.3178 | 0.00016 % | 0.00007 % | |
| 42 | Mo | Molybdenum | 0.9827 | 0.00002 % | 0.00001 % | |
| 47 | Ag | Silver | 1.0365 | 0.00007 % | 0.00003 % | |
| 48 | Cd | Cadmium | 2.0584 | 0.00008 % | 0.00001 % | |
| 50 | Sn | Tin | 3.4910 | 0.00428 % | 0.00050 % | |
| 51 | Sb | Antimony | 1.1930 | < 0.00030 % | (0.0) % | |
| 52 | Те | Tellurium | 3.0949 | < 0.00030 % | (0.0) % | |
| 53 | 1 | lodine | 0.0000 | < 0.00030 % | (0.0) % | |
| 55 | Cs | Cesium | 0.0000 | < 0.00040 % | (0.0) % | |
| 56 | Ba | Barium | 2.3420 | < 0.00020 % | (0.0) % | |
| 57 | La | Lanthanum | 2.2980 | < 0.00020 % | (0.0) % | |
| 58 | Ce | Cerium | 2.1024 | < 0.00020 % | (0.0) % | |
| 59 | Pr | Praseodymium | 8.9735 | 0.00146 % | 0.00012 % | |
| 60 | Nd | Neodymium | 17.4317 | 0.00241 % | 0.00010 % | |
| 72 | Hf | Hafnium | 4.2243 | < 0.00010 % | (0.0) % | |
| 73 | Та | Tantalum | 27.5735 | < 0.00010 % | (0.0) % | |
| 74 | w | Tungsten | 2.0377 | < 0.00002 % | (0.00001) % | |
| 80 | Hg | Mercury | 3.0540 | 0.00004 % | 0.00001 % | |
| 81 | TI | Thallium | 4.5374 | 0.00004 % | 0.00001 % | |
| 82 | Pb | Lead | 6.8112 | 0.00011 % | 0.00001 % | |
| 83 | Bi | Bismuth | 0.0000 | < 0.00010 % | (0.0) % | |
| 90 | Th | Thorium | 7.1449 | 0.00007 % | 0.00001 % | |
| 92 | U | Uranium | 5.0199 | < 0.00010 % | (0.0) % | |
| | | | | | | |





Table 3.B. XRF-analysis on flexible electronic (Sample A, area 3)

| Ζ | Symbol | Element | Norm. Int. | Concentration | Abs. Error | |
|----|--------|--------------|-------------|---------------|-------------|--|
| 12 | Ma | Magnesium | 0.0000 | < 0.0020 % | (0.0) % | |
| 13 | Al | Aluminum | 0.0000 | < 0.0020 % | (0.0) % | |
| 14 | Si | Silicon | 0.0000 | < 0.00051 % | (0.0) % | |
| 15 | P | Phosphorus | 0.0000 | < 0.00030 % | (0.0) % | |
| 16 | S | Sulfur | 0.0000 | < 0.00020 % | (0.0) % | |
| 17 | CI | Chlorine | 270720.9910 | 19.07 % | 0.01 % | |
| 19 | к | Potassium | 5,5596 | 0.00630 % | 0.00024 % | |
| 20 | Ca | Calcium | 12.8424 | < 0.0010 % | (0.0) % | |
| 22 | Ti | Titanium | 7.6467 | 0.00230 % | 0.00007 % | |
| 23 | V | Vanadium | 1.3407 | < 0.00010 % | (0.0) % | |
| 24 | Cr | Chromium | 3.6507 | 0.00025 % | 0.00002 % | |
| 25 | Mn | Manganese | 1.7863 | 0.00016 % | 0.00007 % | |
| 26 | Fe | Iron | 146.3358 | 0.01640 % | 0.00010 % | |
| 27 | Co | Cobalt | 0.6166 | < 0.00030 % | (0.0) % | |
| 28 | Ni | Nickel | 33.4337 | 0.00210 % | 0.00003 % | |
| 29 | Cu | Copper | 13.9648 | 0.00072 % | 0.00003 % | |
| 30 | Zn | Zinc | 25.7379 | 0.00093 % | 0.00002 % | |
| 31 | Ga | Gallium | 3.7489 | 0.00011 % | 0.00001 % | |
| 32 | Ge | Germanium | 0.0000 | < 0.00005 % | (0.0) % | |
| 33 | As | Arsenic | 1.2916 | 0.00002 % | 0.00001 % | |
| 34 | Se | Selenium | 1.6112 | 0.00002 % | 0.00001 % | |
| 35 | Br | Bromine | 2.9298 | 0.00004 % | 0.00001 % | |
| 37 | Rb | Rubidium | 1.2511 | 0.00001 % | 0.00001 % | |
| 38 | Sr | Strontium | 1.9037 | < 0.00005 % | (0.0) % | |
| 39 | Y | Yttrium | 5.9496 | 0.00004 % | 0.00001 % | |
| 40 | Zr | Zirconium | 0.1604 | < 0.00010 % | (0.0) % | |
| 41 | Nb | Niobium | 0.0000 | < 0.00010 % | (0.0) % | |
| 42 | Mo | Molybdenum | 0.8312 | 0.00003 % | 0.00001 % | |
| 47 | Ag | Silver | 0.0000 | < 0.00020 % | (0.0) % | |
| 48 | Cd | Cadmium | 2.1921 | 0.00017 % | 0.00002 % | |
| 50 | Sn | Tin | 3.3198 | 0.00828 % | 0.00094 % | |
| 51 | Sb | Antimony | 0.0000 | < 0.00030 % | (0.0) % | |
| 52 | Те | Tellurium | 3.4218 | < 0.00030 % | (0.0) % | |
| 53 | 1 | lodine | 0.7388 | < 0.00001 % | (0.00001) % | |
| 55 | Cs | Cesium | 0.0000 | < 0.00040 % | (0.0) % | |
| 56 | Ba | Barium | 0.0000 | < 0.00020 % | (0.0) % | |
| 57 | La | Lanthanum | 0.0000 | < 0.00020 % | (0.0) % | |
| 58 | Ce | Cerium | 0.0000 | < 0.00020 % | (0.0) % | |
| 59 | Pr | Praseodymium | 0.2303 | < 0.00012 % | (0.00012) % | |
| 60 | Nd | Neodymium | 0.0000 | < 0.00020 % | (0.0) % | |
| 72 | Hf | Hafnium | 0.5130 | < 0.00010 % | (0.0) % | |
| 73 | Та | Tantalum | 20.1484 | < 0.00010 % | (0.0) % | |
| 74 | W | Tungsten | 0.6391 | < 0.00010 % | (0.0) % | |
| 80 | Hg | Mercury | 2.1332 | 0.00006 % | 0.00001 % | |
| 81 | TI | Thallium | 2.2727 | 0.00005 % | 0.00001 % | |
| 82 | Pb | Lead | 2.0252 | 0.00006 % | 0.00001 % | |
| 83 | Bi | Bismuth | 0.0000 | < 0.00010 % | (0.0) % | |
| 90 | Th | Thorium | 2.6598 | 0.00006 % | 0.00001 % | |
| 92 | U | Uranium | 1.5751 | < 0.00010 % | (0.0) % | |
| | | | | | | |







Figure 2.B. Map of performed XRF analyses for the characterization of sample B





Table 4.B. XRF-analysis on flexible electronic (Sample B, area 1)

| Ζ | Symbol | Element | Norm. Int. | Concentration | Abs. Error | 2 |
|-------|--------|--------------|-----------------|---------------|------------|---|
| 12 | Ma | Magnesium | 0.0000 | < 0.0020 % | (0.0) % | |
| 13 | AI | Aluminum | 91.3854 | < 0.0020 % | (0.0) % | |
| 14 | Si | Silicon | 955,3650 | 0.5219 % | 0.0009 % | |
| 15 | P | Phosphorus | 25.3750 | 0.00533 % | 0.00017 % | |
| 16 | S | Sulfur | 3865,2044 | 0.3858 % | 0.0003 % | |
| 17 | CI | Chlorine | 321.3761 | 0.01268 % | 0.00004 % | |
| 19 | K | Potassium | 64.0969 | 0.02909 % | 0.00029 % | |
| 20 | Ca | Calcium | 291.7725 | 0.07120 % | 0.00032 % | |
| 22 | Ti | Titanium | 270.7637 | 0.03110 % | 0.00014 % | |
| 23 | V | Vanadium | 39.4186 | 0.00301 % | 0.00009 % | |
| 24 | Cr | Chromium | 58.6370 | 0.00240 % | 0.00005 % | |
| 25 | Mn | Manganese | 30443.7852 | 1.144 % | 0.001 % | |
| 26 | Fe | Iron | 28800.9340 | 1.710 % | 0.001 % | |
| 27 | Co | Cobalt | 3.8002 | 0.00016 % | 0.00002 % | |
| 28 | Ni | Nickel | 53.2246 | 0.00212 % | 0.00003 % | |
| 29 | Cu | Copper | 722.0398 | 0.02312 % | 0.00007 % | |
| 30 | Zn | Zinc | 59.0909 | 0.00132 % | 0.00002 % | |
| 31 | Ga | Gallium | 1.3793 | 0.00003 % | 0.00001 % | |
| 32 | Ge | Germanium | 0.0000 | < 0.00005 % | (0.0) % | |
| 33 | As | Arsenic | 1.7734 | 0.00002 % | 0.00001 % | |
| 34 | Se | Selenium | 1.1429 | 0.00001 % | 0.00001 % | |
| 35 | Br | Bromine | 5.1738 | 0.00005 % | 0.00001 % | |
| 37 | Rb | Rubidium | 10.4546 | 0.00006 % | 0.00001 % | |
| 38 | Sr | Strontium | 99.0798 | 0.00030 % | 0.00001 % | |
| 39 | Y | Yttrium | 5.8382 | 0.00003 % | 0.00001 % | |
| 40 | Zr | Zirconium | 0.2563 | < 0.00010 % | (0.0) % | |
| 41 | Nb | Niobium | 0.0000 | < 0.00010 % | (0.0) % | |
| 42 | Mo | Molybdenum | 1.5034 | 0.00007 % | 0.00001 % | |
| 47 | Ag | Silver | 0.0000 | < 0.00020 % | (0.0) % | |
| 48 | Cd | Cadmium | 2.0407 | 0.00011 % | 0.00002 % | |
| 50 | Sn | Tin | 2.7209 | 0.00406 % | 0.00057 % | |
| 51 | Sb | Antimony | 0.8035 | < 0.00030 % | (0.0) % | |
| 52 | Те | Tellurium | 3.3223 | < 0.00030 % | (0.0) % | |
| 53 | 1 | lodine | 0.0000 | < 0.00030 % | (0.0) % | |
| 55 | Cs | Cesium | 0.0000 | < 0.00040 % | (0.0) % | |
| 56 | Ba | Barium | 5.4468 | < 0.00020 % | (0.0) % | |
| 57 | La | Lanthanum | 0.0000 | < 0.00020 % | (0.0) % | |
| 58 | Ce | Cerium | 2.2132 | < 0.00020 % | (0.0) % | |
| 59 | Pr | Praseodymium | 19.1607 | 0.00343 % | 0.00017 % | |
| 60 | Nd | Neodymium | 33.5189 | 0.00496 % | 0.00014 % | |
| 72 | Hf | Hafnium | 2.7361 | < 0.00010 % | (0.0) % | |
| 73 | Та | Tantalum | 23.9550 | < 0.00010 % | (0.0) % | |
| 74 | W | Tungsten | 3.6538 | 0.00007 % | 0.00001 % | |
| 80 | Hg | Mercury | 1.8804 | 0.00003 % | 0.00001 % | |
| 81 | TI | Thallium | 5,2921 | 0.00007 % | 0.00001 % | |
| 82 | Pb | Lead | 10.0493 | 0.00026 % | 0.00001 % | |
| 83 | Bi | Bismuth | 0.0000 | < 0.00010 % | (0.0) % | |
| 90 | Th | Thorium | 11.2372 | 0.00016 % | 0.00001 % | |
| 92 | U | Uranium | 3.5524 | < 0.00010 % | (0.0) % | |
| 25.5% | 367-33 | | N THE CONSERVED | | NE 177 | |





| Z | Symbol | Element | Norm. Int. | Concentration | Abs. Error | |
|----|--------|--------------|------------|---------------|-------------|--|
| 12 | Mg | Magnesium | 0.0000 | < 0.0020 % | (0.0) % | |
| 13 | AŬ | Aluminum | 56.0221 | < 0.0020 % | (0.0) % | |
| 14 | Si | Silicon | 879.9840 | 0.4786 % | 0.0009 % | |
| 15 | P | Phosphorus | 3.5905 | 0.00075 % | 0.00020 % | |
| 16 | S | Sulfur | 6135.8149 | 0.6122 % | 0.0005 % | |
| 17 | CI | Chlorine | 599.3317 | 0.02586 % | 0.00006 % | |
| 19 | к | Potassium | 336.4141 | 0.1545 % | 0.0005 % | |
| 20 | Ca | Calcium | 81.9894 | 0.01036 % | 0.00010 % | |
| 22 | Ti | Titanium | 225.4893 | 0.02652 % | 0.00013 % | |
| 23 | V | Vanadium | 34.9249 | 0.00271 % | 0.00008 % | |
| 24 | Cr | Chromium | 48.3154 | 0.00199 % | 0.00004 % | |
| 25 | Mn | Manganese | 25404.2805 | 0.9592 % | 0.0006 % | |
| 26 | Fe | Iron | 24484.8954 | 1.483 % | 0.001 % | |
| 27 | Co | Cobalt | 4.1156 | 0.00032 % | 0.00004 % | |
| 28 | Ni | Nickel | 47.2170 | 0.00178 % | 0.00003 % | |
| 29 | Cu | Copper | 611.1902 | 0.01864 % | 0.00006 % | |
| 30 | Zn | Zinc | 53.6945 | 0.00114 % | 0.00001 % | |
| 31 | Ga | Gallium | 4.5156 | 0.00008 % | 0.00001 % | |
| 32 | Ge | Germanium | 1.5509 | 0.00002 % | 0.00001 % | |
| 33 | As | Arsenic | 1.2933 | 0.00001 % | 0.00001 % | |
| 34 | Se | Selenium | 2.9045 | 0.00003 % | 0.00001 % | |
| 35 | Br | Bromine | 8.1709 | 0.00007 % | 0.00001 % | |
| 37 | Rb | Rubidium | 8.6477 | 0.00004 % | 0.00001 % | |
| 38 | Sr | Strontium | 92.4721 | 0.00024 % | 0.00001 % | |
| 39 | Y | Yttrium | 7,1790 | 0.00003 % | 0.00001 % | |
| 40 | Zr | Zirconium | 3.4229 | < 0.00010 % | (0.0) % | |
| 41 | Nb | Niobium | 0.2721 | < 0.00016 % | (0.00015) % | |
| 42 | Mo | Molybdenum | 1.6669 | 0.00007 % | 0.00001 % | |
| 47 | Ag | Silver | 734.7557 | 0.06899 % | 0.00015 % | |
| 48 | Cď | Cadmium | 2.2654 | 0.00012 % | 0.00002 % | |
| 50 | Sn | Tin | 0.0000 | < 0.00030 % | (0.0) % | |
| 51 | Sb | Antimony | 0.5490 | < 0.00030 % | (0.0) % | |
| 52 | Те | Tellurium | 4.2044 | < 0.00030 % | (0.0) % | |
| 53 | 1 | lodine | 1.3899 | 0.00005 % | 0.00002 % | |
| 55 | Cs | Cesium | 0.0000 | < 0.00040 % | (0.0) % | |
| 56 | Ba | Barium | 4.2044 | < 0.00020 % | (0.0) % | |
| 57 | La | Lanthanum | 0.0000 | < 0.00020 % | (0.0) % | |
| 58 | Ce | Cerium | 2.2308 | < 0.00020 % | (0.0) % | |
| 59 | Pr | Praseodymium | 14.8152 | 0.00264 % | 0.00016 % | |
| 60 | Nd | Neodymium | 28.7226 | 0.00434 % | 0.00013 % | |
| 72 | Hf | Hafnium | 3.9950 | < 0.00010 % | (0.0) % | |
| 73 | Та | Tantalum | 20.9725 | < 0.00010 % | (0.0) % | |
| 74 | W | Tungsten | 3.1675 | 0.00005 % | 0.00001 % | |
| 80 | Hg | Mercury | 1.0741 | < 0.00002 % | (0.00001) % | |
| 81 | ΤĬ | Thallium | 3.9676 | 0.00005 % | 0.00001 % | |
| 82 | Pb | Lead | 9.1957 | 0.00023 % | 0.00001 % | |
| 83 | Bi | Bismuth | 0.0000 | < 0.00010 % | (0.0) % | |
| 90 | Th | Thorium | 9.9739 | 0.00013 % | 0.00001 % | |
| 92 | U | Uranium | 3.6662 | < 0.00010 % | (0.0) % | |
| | | | | | | |

Table 5.B. XRF-analysis on flexible electronic (Sample B, area 2)

